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## **Biot-Based Geoacoustic Investigation of Lake Arkabutla, Mississippi**

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and Rodney L. Leist

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# **Biot-Based Geoacoustic Investigation of Lake Arkabutla, Mississippi**

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# Preface

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The work described in this report was performed during the period March to July 1999 by Mr. Richard G. McGee, senior coastal engineer, Evans-Hamilton, Inc., Seattle, WA. The work was performed under Contract No. DACW39-92-D-0012 and funded by the Earthquake Engineering (EQEN) Research Program project, "Geophysical Methods for Site Characterization and Measurement of Seismic Properties," Work Unit No. 33014.

This report was prepared by Mr. McGee and his staff at Evans-Hamilton, Principal Investigators for the EQEN Research Project, and Messrs. Robert F. Ballard, Jr., and Rodney L. Leist, members of the staff of U.S. Army Engineer Research and Development Center (ERDC), Vicksburg, MS, Earthquake Engineering and Geosciences Division (EEGD), Geotechnical Laboratory (GL). This work was performed under the general supervision of Dr. Lillian D. Wakeley, Acting Chief, EEGD, and Dr. Michael J. O'Connor, Director, GL. Dr. Mary Ellen Hynes was EQEN Project Manager.

At the time of publication of this report, Director of ERDC was Dr. James R. Houston, and Commander was COL James S. Weller, EN.

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# Conversion Factors, Non-SI to SI Units of Measurement

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Non-SI units of measurement used in this report can be converted to SI units as follows:

Multiply	By	To Obtain
cubic yards	0.7645	cubic meters
feet	0.3048	meters



# 1 Introduction

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The Earthquake Engineering Research Program embodies several work units, one of which is entitled "Geophysical Methods for Site Characterization and Measurement of In Situ Properties." Its objective is to develop geophysical procedures that provide broader, more economic site coverage while determining more engineering parameters than before possible. In previous years, work has concentrated on developing techniques for use downstream of dams. However, safe, cost-effective design of U.S. Army Corps facilities has been limited by lack of accurate information on upstream site conditions. The need exists for development of in situ techniques for more accurately determining upstream site conditions relating to earthquake response. In view of the fact that downstream data are incorrectly extrapolated upstream, new innovative waterborne geophysical techniques must be developed to alleviate this problem. An acoustic impedance technique reported by McGee, Ballard, and Caulfield (1995), developed under the Dredging Research Program, appears ripe for further development for this application. A technically significant upgrade to this technique is the implementation of a Biot theory approach in assessing acoustic-sediment interactions in porous, saturated media. Ramifications of the Biot theory may aid engineers in accurately assessing liquefaction potential of Corps structures. This pilot study program has been conducted to evaluate new techniques to quantitatively assess sediment conditions upstream of man-made dams.

## Site Selection

Arkabutla Dam and reservoir was selected as the site to demonstrate the feasibility of upstream site characterization using waterborne acoustic techniques for a variety of reasons: proximity to the New Madrid seismic zone, existing site documentation (borings in the reservoir), support from U.S. Army Engineer District, Vicksburg, and mobilization cost. Further, Arkabutla Dam is the subject of a seismic stability analysis.

## General History of Arkabutla Lake

Arkabutla Lake Project is located in northwestern Mississippi on the Coldwater River, a tributary of the Yazoo River. The dam is one of four flood control dams in the Yazoo River Basin, Mississippi. The dam is of earthfill construction,

approximately 10,700 ft long with a crown width of 40 ft. Approximately 4,460,000 cu yd of embankment materials were used in constructing the dam. Slopes are protected by riprap. Maximum height above the valley floor is 67 ft. The outlet works is located near the south abutment of the main dam. It consists of a concrete approach, three-gated control structure, transition, single-barrel conduit, chute, and stilling basin. Further detailed information, if desired, is available from the Vicksburg District.

## 2 Approach

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The methodology used to quantitatively assess the characteristics of the sediments within Lake Arkabutla is a modified seismic reflection technique that relates the engineering properties of sediments to acoustic impedance by precisely determining the reflection coefficient at each reflection horizon. To accomplish this task, a very rigorous Biot-based geoacoustic modeling program allowing for detailed investigation of up to thirteen physical fluid/sediment properties is applied to the acoustic data. The Biot theory and how it is specifically applied within the Lake Arkabutla program is provided herein.

### Acoustic Subbottom Profile Data

Acoustic subbottom profile data (SBP) were collected at 1- and 4-kHz frequencies to map sediment conditions throughout the survey. Figure 1 is an example of subbottom imagery from Lake Arkabutla. It graphically shows the capability of subbottom profiling in providing stratigraphic and lithological assessment of bottom and subbottom sediment environments.

As the transmitted acoustic signal travels downward through the water column, reflections are generated at boundaries between two layers of differing material properties. In Figure 1, reflections are detected at the lakebed and in the subbottom at stratigraphic interfaces. This reflection record is actually from the approach channel to the dam outlet works. It shows recent sediment accumulation since lake formation as well as relic streambed sedimentation represented by the deeper reflection horizons.

A more typical subbottom image from Lake Arkabutla, Figure 2, shows an east-west survey line starting above the riprap blanket at the toe of the dam. Surveying away from the dam, a layer of unconsolidated sediment overlays an acoustically impenetrable horizon probably comprised of the native soil prior to dam construction.

These data are geocoded with accurate position data allowing for delineation of the horizontal and vertical extents of all unique sediment units. Another feature of these data is the contrasting colors (yellow to red color ramp) representing relative echo intensity. The higher the contrast, the greater the change in material properties. For example, a hard bottom would cause a high intensity (red to black) echo whereas the echo from a soft muddy bottom would be a low intensity (yellow hue). After calibration of the acoustic systems, these same data are

processed analytically to derive quantitative sediment properties such as density or porosity.

## Reflectivity and Acoustic Impedance

Acoustic impedance,  $Z$ , is defined as the product of the seismic transmission velocity and the density of a material and basically represents the influence of a medium's characteristics on reflected and transmitted waves. Many geotechnical properties such as porosity, density, mean grain size, bulk modulus, etc., exhibit excellent correlation with impedance. It is possible, therefore, with data of a sufficient signal-to-noise (S/N) ratio, to predict geotechnical properties from normal reflectivity data through calculations of the sediment acoustic impedance. For example, acoustic impedance of the bottom surface sediment unit is related to the reflection coefficient derived at the water-sediment interface through the Zoeppritz equation (Zoeppritz 1919)

$$Z_2 = Z_1 \frac{(1 + R)}{(1 - R)} \quad (1)$$

where

$Z_2$  = impedance of second layer (the bottom sediment surface)

$Z_1$  = impedance of the overlying layer (in this case the water column)

$R$  = reflection coefficient at water/sediment interface.

Since the sound velocity and density of water are known,  $Z_1$  can be readily calculated. Therefore, to assess bottom impedance ( $Z_2$ ) one must first accurately determine the reflection coefficient ( $R$ ) at the water-sediment interface. This is computed using what is referred to in underwater acoustics as the *sonar equation*. The *sonar equation*, discussed thoroughly by Urick (1983), describes the quantitative effects on sonar equipment created by many phenomena peculiar to underwater sound production. This equation is a design and prediction tool for underwater sound applications and relates the effects of the medium, target, and equipment. The general sonar equation is given as follows:

$$S_R = SL - N_w - N_{hyd} + DI + BL + N_A \quad (2)$$

where

$S_R$  = bottom reflection energy at receiver, db

$SL$  = total energy of source, db

$N_w$  =  $20 \times \log_{10}$  (range, meters), db (transmission loss due to spherical spreading along the path of propagation)

$N_{hyd}$  = receiver sensitivity, db

$N_A$  = amplifier gain, db

DI = directivity index of receiving array, db (function of transducer beam pattern)

BL = bottom loss, db =  $20 \log_{10}(R)$

R = reflection coefficient

Bottom loss, *BL*, is evaluated by rearranging Equation 2:

$$BL = S_R + N_{hyd} - SL + N_w - N_A - DI \quad (3)$$

Since all terms on the right side of the equation are either measured directly or determined through precise equipment calibrations, *BL*, and therefore the surface reflection coefficient ( $BL = 20 \log_{10} R$ ) and acoustic impedance (Equation 1), can be determined. If the desired result is an assessment of the bottom surface characteristics, the acoustic solution is complete. All that remains is the correlation between the acoustic parameters and physical sediment properties through geoacoustic relationships. This correlation is accomplished using a Biot-based geoacoustic modeling program.

For Lake Arkabutla, *BL* is calculated on all 4-kHz reflection data providing continuous survey line coverage of lakebed sediment conditions.

## Biot-based Geoacoustic Modeling (BBSS)

The Biot theory (1956) was developed to explain acoustic behavior of saturated sedimentary materials accumulating on the seafloor. The applicability of the Biot theory to surficial marine sediments has been demonstrated by Stoll and Bryan (1970). Ogushwitz (1985) further assessed the applicability of the theory to the entire suite of sedimentary materials, from surficial materials with porosities as high as 90 percent, to well-consolidated materials with porosities as low as 1 percent.

Saturated sediment consists of a porous assemblage of sediment grains (the "skeletal frame"), whose interconnected pores are filled with water or gas (the "pore fluid"). Biot (1956) devised a theoretical model to describe the acoustic behavior in such a material. The Biot model treats both the individual and coupled behavior of the frame and pore fluid. Energy loss is considered to be caused by the inelasticity of the skeletal frame and by the viscosity of the pore fluid as it moves relative to the frame. The model predicts that sound velocity and attenuation in sediment will depend on frequency, the elastic properties of the sediment grains and pore fluid, material porosity, mean grain size, permeability, and effective stress.

Evans-Hamilton, Inc. (EHI) and Ogushwitz developed the *Biot-Based Synthetic Seismogram* (BBSS) program for conducting Biot-based geoacoustic modeling. The purpose of this program is to correlate measured acoustic responses with corresponding sediment properties. The BBSS program specifies values for 13 physical parameters describing the fluid, grains, and frame properties listed in Table 1. Ogushwitz's (1985) paper provides detailed guidelines for specifying

<b>Table 1 Biot Model Input Parameters</b>	
<b>Fluid Properties</b>	
Density of pore fluid	g/cm <sup>3</sup>
Bulk modulus of pore fluid	dyne/cm <sup>2</sup>
Viscosity of pore fluid	P
<b>Grain Properties</b>	
Density of sediment grains	g/cm <sup>3</sup>
Bulk modulus of grains	dyne/cm <sup>2</sup>
Shear modulus of grains	dyne/cm <sup>2</sup>
Mean grain size	Cm
<b>Frame Properties</b>	
Porosity	Dimensionless
Dynamic permeability	cm/sec
Structure factor	Dimensionless
Pore size parameter	Cm
Complex bulk modulus of frame	dyne/cm <sup>2</sup>
Complex shear modulus of frame	dyne/cm <sup>2</sup>

values of these parameters within the BBSS program. EHI applied the BBSS program to the 4-khz acoustic reflection data from Lake Arkabutla, in conjunction with inferred sediment property information, to develop the geoacoustic parameters necessary to create synthetic seismograms based on the specific outputs of the BBSS program listed in Table 2. A conceptual schematic of this process is presented as Figure 3.

<b>Table 2 Biot Model Acoustic Property Outputs</b>	
<b>Properties</b>	<b>Units</b>
Wave speed	M/SEC
Absorption	DB/M
Impedance	MKS
Reflection Coefficient	None
Signal Amplitude	Volts
Phase	Degrees

## Assessment of Sediment Properties within BBSS

As shown in Figure 3, acoustic impedance,  $Z$ , has been related to sediment bulk density. Within the skeletal frame parameters, porosity and the frame moduli (Table 1) are the dominant properties affecting wave propagation in water-saturated sediments (Ogushwitz 1985). Estimates of the fluid and grain properties were arrived at based on standard water properties and from limited core data, respectively. The elastic constants and porosity values were then

iterated to produce synthetic seismograms matching the actual recorded data. A relationship was then developed between measured acoustic impedance and bulk density based on the relation between porosity and specific gravity. The density function shown in Figure 3 is the same relationship used for the Lake Arkabutla study.

## 3 Survey and Equipment

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### Survey

A 1000-ft swath of high resolution subbottom profile (SBP) data, sidescan sonar (SSS) data, and high frequency bathymetric data were collected along the entire north/south (N/S) length of the upstream side of Arkabutla Dam. Figures 4 and 5 present actual survey track lines for the 1- and 4-kHz geophysical systems, respectively. 4-kHz SBP data were collected along three parallel N/S transects approximately 500 ft apart, and thirty-three East/West transects at approximately 200 ft apart. This provides a balanced matrix of data for producing an accurate spatial representation of lakebed sediments. Additionally, 1-kHz SBP data were collected along the two easternmost survey lines. SSS data were collected along the three N/S 4-kHz tracklines to continuously map lakebed features and structural appurtenances to the dam.

The survey was conducted on March 29 through 31. Weather conditions were rain with brisk wind producing 0- to 1-ft wind chop on the reservoir.

### Instrumentation

Due to acoustic interference between systems, the subbottom and SSS surveys were conducted independently. All geophysical data were directly interfaced with the survey vessel's positioning system. Specific instrumentation is listed in Table 3. A brief description of each instrument is provided below.

### Survey vessel

The survey was conducted aboard the survey vessel *Nancy Kay* owned and operated by DIMCO, Inc., Vicksburg, MS. The survey vessel is shown as mobilized for the Arkabutla Lake survey in Figure 6.

### Navigation

A Starlink Differential Global Positioning System (DGPS) was used for positioning. Real-time differential corrections were obtained from nearest Coast Guard beacon installation, improving horizontal positional accuracy to less than



<b>Table 3 Instrumentation</b>		
<b>System</b>	<b>Model</b>	<b>Comments</b>
Navigation	Starlink GPS	Differential GPS with approximately $\pm 2$ m accuracy
Navigation Software	HYPACK	Position logging and survey control for all systems
High-frequency echosounder	Ross Laboratories Smartsounder	200 kHz
Sidescan sonar	EG&G SMS-260TH W/272-TD Tow fish	100- and 500-kHz dual frequency sonar system
High-resolution subbottom profiling (SBP) system	Datasonics SBP-5000	4- and 7-kHz operations
Digital Acquisition System	Triton Isis Data Acquisition and Processing System	Dual processor high-speed acquisition system used to collect all geophysical data.

$\pm 2$  m RMS. Survey navigation, control, and data acquisition was accomplished using the HYPACK surveying package by Coastal Oceanographics. This system received data from the DGPS and fathometer, performed the appropriate geodetic transformations, and then transmitted corrected position and depth information to other instrument packages, such as the Isis system, aboard the *Nancy Kay*. Coordinates used for this investigation are UTM, Zone 15, and are in units of survey feet.

### **Subbottom profiler**

The higher-frequency acoustic subbottom reflection records were generated using a Datasonics SBP-5000 high-resolution "pinger" system. The system was operated at 4-kHz to optimize for resolution and depth penetration beneath the upper lithological unit. To identify the acoustic data basement, a lower frequency acoustic system referred to as a 'boomer' operated below 1-kHz was used concurrently. These low-frequency data have poor vertical resolution but allow for greater depth of penetration than the pinger system. No statistical data analysis was performed on the boomer data, however, the data proved critical in verifying data basement.

### **Sidescan sonar**

An Edgetech Model SMS-260TH image correcting sidescan sonar system with a dual frequency (100- and 500-kHz) transducer tow fish was used for all sidescan operations. The system was operated at 500-kHz with a range of 75 m per side. Figure 7 shows the Model 272-TD dual frequency tow fish being deployed over the bow of the *Nancy Kay*. Sonar data were provided directly to the shipboard Edgetech graphic recorder and in analog form to the ISIS digital acquisition system for real-time quality control, display, and data storage. Figure 8 shows all acquisition system components aboard the *Nancy Kay*.

## **Digital data acquisition system**

The ISIS shipboard data acquisition and image processing system was used to acquire, store, and process all subbottom and side scan data. The Isis system also acts as an interface between the navigation and geophysical systems providing real-time geocoding of all data. Multiple channels of data were recorded with 16-bit analog to digital converters operating through multiple sessions of Isis. The system was capable of acquisition rates of nearly 33 kHz per channel. Graphic displays (see Figure 8) provided real-time quality control of all data during acquisition.

## **4 Data Processing and Mapping**

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### **Acoustic Reflection Data Records**

Appendix A contains a copy records of the 1- and 4-kHz subbottom profile data. The survey track lines in Figures 4 and 5 include the filenames and selected ping numbers to correlate geographic location with the data plots. Filenames are shown where they begin (at ping 0) with ping numbers annotated every 400 pings. Shown along with the filename is the CDROM archive disk number on which the actual data resides (i.e., D01). Survey direction is in order of increasing ping number.

As stated in Chapter 3, subbottom data were collected at 4-kHz for the entire survey for the purpose of characterizing the uppermost sediment. To verify data basement, a 'boomer' system was operate below 1-kHz along the easternmost north-south survey line (Figure 4). For most of the survey, acoustic penetration was limited to the bottom of the uppermost sediment unit. The confining layer is inferred to be the native soil that was exposed prior to flooding of the reservoir. The boomer data did not achieve any more penetration than the 4-kHz system. Figure 9 shows a comparison between these two data sets. At both frequencies the same reflection horizon confines acoustic penetration. The only location in the survey area where considerable acoustic penetration was obtained (Figure 1) was within the banks of the approach channel to the intake structure.

### **Bathymetry**

Data from the 200-kHz fathometer was used to create a bathymetric surface grid and contour map of the survey area. The bathymetry map (Figure 10) shows a relatively flat surface. The most significant relief variation is between 14100500N and 14101000N near the intake tower. The 20- by 20-ft resolution digital bathymetric grid was used to create isometric surfaces, sediment thickness maps and for the overlays of sediment property data and the surface feature maps.

## Side Scan Sonar Mosaic

The digital SSS data were processed to create a 0.2-m resolution geocorrected digital mosaic of the entire survey area. A small version of the mosaic is presented here as Figure 11. The SSS data supports the subbottom findings showing a remarkably uniform, low backscatter reflection surface indicative of a soft, smooth, featureless lakebed. At places the more competent native materials extrude through the recent sediment deposits as shown by darker reflection patches on Figure 11. The mosaic was useful in mapping the extents of the submerged riprap blanket covering the upstream face of the dam below the water surface. Any future surveys should include full bottom SSS imagery to assess the spatial distribution of surficial sediment conditions.

Figure 12 shows a close-up view of the intake appurtenances, i.e., wing walls, intake passages, and the bottom features in the near vicinity of the structure.

The mosaic is available as a GeoTiff image importable directly into ArcInfo GIS. No detailed interpretation of the side scan imagery was performed as part of this investigation.

## 5 Geoacoustic Modeling

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Using calibration procedures for data with high S/N ratios, the 4-kHz acoustic reflection data were processed to provide estimates of the porosity, density, and other associated properties of the sediments found in Lake Arkabutla. Calibrations were performed to precisely assess operational parameters of the acoustic equipment. Then, in conjunction with known sediment properties, the geoacoustic parameters needed to relate acoustic impedance with porosity and density were developed. The calibrations procedures are described briefly below.

### Equipment Calibration: Sources and Receivers

Equipment calibrations involve direct measurements to determine the precise transmit and receiving transducer sensitivities. Using the sonar equation (Equation 2), determination of transmitter response and total energy at the source, source level ( $SL$ ), and receiving array sensitivity,  $N_{hydr}$ , was accomplished by rearranging the equation to solve for  $SL$ . The specific field procedures and data analysis methodology followed precisely as described in McGee et al. (1995). Table 4 lists specific equipment parameters measured for the 4-kHz acoustic reflection system. These values were used as input parameters to the BBSS geoacoustic-modeling program for scaling of output synthetic seismograms and to the bottom sediment analysis program (BSED51) used for inversion of the acoustic reflection data to sediment properties.

<b>Table 4</b> <b>Equipment Parameters: SBP-5000</b>	
Frequency, kHz	4
Output Attenuation, dB	-10
SIU Attenuation Setting	2
Pulse Length, ms	0.2
Wavelet Sample Bin Size	22
Source Level, $SL$ , dB re 1 dyne/cm <sup>2</sup>	100
Receiver Sensitivity, $N_{hydr}$ , dB re 1 dyne/cm <sup>2</sup>	-72

## Determination of Bottom Loss and Surface Reflection Coefficient

Characterization of the sediment surface begins by evaluating the acoustic bottom loss, BL, according to Equation 3. By substituting into Equation 3 the equipment parameters from Table 4 ( $SL$  and  $N_{hydr}$ ,  $N_w$ , and  $DI$ ), and evaluating the surface data throughout the survey area, a contiguous assessment of sediment acoustic response is accomplished. The acoustic solution for the bottom sediments is now complete. For the surface data, the remaining task involves correlation of acoustic response to sediment properties, hence establishing the geoacoustic calibration. All geoacoustic assessments are primarily related to the acoustic impedance,  $Z_2$ .

## Biot Modeling

### Biot parameters

As stated in Chapter 2, EHI developed the BBSS program for conducting Biot-based geoacoustic modeling to correlate measured acoustic responses with in situ sediment properties. These properties are typically confirmed through sediment core analysis. Specific implementation of the program is through a framework of forward modeling requiring correlation of predicted acoustic responses based on specified sediment conditions with actual measured acoustic returns. Known or inferred sediment parameters (Table 1) are used as inputs to the model and the desired quantities are manipulated to give a matching seismic response to the actual acoustic data (Table 2). Verification is provided by coring and sample analysis. For the Arkabutla study, very limited sediment data were available. Core data, included in Appendix B, provided soil and sediment properties in terms of the Unified Soil Classification System, i.e., soil type, Atterburg limits, moisture contents, etc., but no laboratory measurements of any of the thirteen physical Biot parameters. Although quantitative property information was not available, the information did provide general constraints within which the Biot theory could be used in a predictive mode.

### Sediment categorization

Table 5 presents the basic categories used to report sediment conditions in Lake Arkabutla. Sediment categories are grouped according to a density range associated with sediment types. These definitions were developed by correlating acoustic response characteristics with the available core data through the BBSS program. Given the lack of sample data, sediment bulk density is considered the most reliable sediment parameter to predict. Sediment density is closely related to the elasticity of the sediments and can be calculated from acoustic impedance; a parameter that represents the influence of the medium's characteristics on reflected and transmitted waves. For all categories density is the most accurate to derive acoustically and best represents insitu conditions.

<b>Table 5 Sediment Description</b>	
<b>Density, g/cm<sup>3</sup></b>	<b>Basic Sediment Description</b>
< 1.2	Fluidized mud, very soft
1.2 - 1.4	Unconsolidated mud, saturated clay, silt
1.4 - 1.7	Clay-silt, clay-silt-sand mixtures
1.7 - 2.0	Stiff clayey sand, silty sand, fine sand
2.0 - 2.2	Dense clays, unsaturated sediments, possible organics
N/A	Riprap blanket

For this discussion, fluid mud is defined as sediments with density values less than 1.2 g/cm<sup>3</sup>. Sediments below 1.2 g/cm<sup>3</sup> possess physical properties typical of fluidized unconsolidated sediments. These sediments were modeled with porosities greater than 0.85 and negligible frame and shear moduli (specific modeling results are discussed later). Sediments in the 1.2 - 1.4 g/cm<sup>3</sup> range responded geoacoustically as an inelastic frame (reasonable frame moduli) and have physical properties representative of freshwater clays and silts.

The sediments with densities higher than 2 g/cm<sup>3</sup> are potentially dense clays or even unsaturated sediments present before the filling of the reservoir. As will be shown in the next section, acoustic responses from these sediments were often outside the response range typical of marine sediments.

## Modeling results

After reviewing all the data, three sites were chosen to represent the different acoustic environments found underneath Lake Arkabutla. These sites were selected to demonstrate the ability of the technique to meet the objectives of this investigation as well as its potential limitations.

**Site Ark16a.** This site is located immediately upstream (east) of the intake tower within the confines of a submerged entrance channel along survey file AR040016 in Figure 5 (refer also to Figure 24 for actual location). Figure 1 is the actual 4-kHz subbottom profile data from which the model site was selected. The model site was chosen near the area of deepest acoustic penetration. As can be seen by this reflection profile (Figures 1 and 24), nearly 17 ft of acoustic penetration was achieved at 4-kHz. It is likely this feature was part of the relic channel where erosion and depositional cycles occurred prior to filling the reservoir. An actual acoustic signal representative of this depositional environment is shown in Figure 13.

A five-layer model (water column plus four sediment layers) was required to match the data. An acceptable calibration (Figure 13), requires that actual and predicted signal amplitude and phase match accordingly. The synthetic seismogram (red line in Figure 13) is produced after convolution of a field-measured source wavelet (accomplished during equipment calibration) with the reflection

sequence modeled according to Biot theory. Table 6 presents the specific input parameters required for the BBSS model.

<b>Table 6 Blot Model Geoacoustic Input Parameters; Site Ark16a</b>					
	<b>Layer 1</b>	<b>Layer 2</b>	<b>Layer 3</b>	<b>Layer 4</b>	<b>Layer 5</b>
<b>Label</b>	Water	Soft Mud	Clay-silt-sand	Sand-silt-clay	Consolidated Sediment
Travel Time to bottom of layer, ms	12.20	13.30	16.15	18.54	N/A
<b>Fluid</b>					
Fluid Density, g/cm <sup>3</sup>	1.0	1.0	1.0	1.0	1.0
Fluid Bulk Modulus, dynes/cm <sup>2</sup> , xE+11	0.215	0.215	0.215	0.215	0.215
Fluid Viscosity	0.019	0.019	0.019	0.019	0.019
<b>Grain</b>					
Grain Density, dynes/cm <sup>2</sup>		2.53	2.65	2.65	2.65
Grain Bulk Modulus (Real), xE+11		5.40	4.50	4.50	3.64
Grain Shear Modulus (Real), xE+11		2.70	2.10	2.10	1.80
Mean Grain Size, cm		0.0016	0.0062	0.016	0.016
<b>Frame</b>					
Porosity		0.84	0.55	0.47	0.36
Permeability, cm/sec, xE-05		0.04	0.003	0.0007	0.00006
Frame Bulk Modulus (Real), dynes/cm <sup>2</sup> , xE+09		No Frame	2.50	2.50	102.0
Frame Bulk Modulus (Imag), dynes/cm <sup>2</sup> , xE+09		No Frame	0.027	0.027	1.12
Frame Shear Modulus (Real), dynes/cm <sup>2</sup> , xE+09		No Frame	1.15	1.15	47.0
Frame Shear Modulus (Imag), dynes/cm <sup>2</sup> , xE+09		No Frame	0.037	0.037	1.50

Sediment layers range from soft muddy sediments to a dense, high impedance layer considered the acoustic 'basement.' The soft mud blankets the lake-bed and is found throughout the survey area. This mud represents recent deposition and shows properties typical to unconsolidated fine-grained sediments. This layer was modeled with negligible frame and shear bulk moduli which account for the lack of shear strength normally found in consolidated sediment materials. Porosity was determined to be 0.84 and wave velocity and acoustic impedance 1429 m/sec (indicates near saturation) and 1778 mks, respectively.

Underlying this soft mud layer is a unit of clay/silt/sand (Table 6, Layer 3) with a porosity of 0.55. This results in a high-impedance contrast with the upper layer. Wave velocities increased to 1539 m/sec. Average bulk density modeled at 1.74 g/cm<sup>3</sup>.

Beneath the clay/silt/sand unit is a more competent layer (Table 6, Layer 4). An increase in density from 1.74 g/cm<sup>3</sup> to 1.87 g/cm<sup>3</sup> could result from a higher percentage of sand in the material.



A high impedance layer ( $> 6300$  mks), represented by the high-amplitude reflector in Figure 13, is the confining acoustic interface and was modeled as a consolidated sediment with very high frame bulk and shear moduli (Layer 5 in Table 6). Polarity of the reflection coefficient remained positive indicating an increasing impedance environment (i.e., a harder material than the overburden sediment). No penetration was achieved below this layer with any of the acoustic systems.

The sediment cores did not provide enough information to establish absolute verification of the model. However, based on past experience and general guidance regarding the likely sediment environment at Lake Arkabutla, the results should be considered reasonable estimates of actual conditions. Except for pockets of trapped gas (i.e., organics) and consolidated, unsaturated sediments, estimates of the acoustic responses (impedance, velocity, phase, and reflection coefficient) should be accurate.

**Site Ark14a.** This site represents a potential difficulty in using normal-incidence reflection techniques where the sediments were previously exposed native soils submerged after filling of a reservoir. Figure 2 from Chapter 1 is the profile data from line 14 and shows a soft mud layer overlying a highly reflective and acoustically impenetrable layer at Model site Ark14a (actual location shown in Figure 23). Figure 14 shows the upper sediment unit modeling as a soft mud identical to the uppermost unit model at site. Acoustic penetration is arrested at the bottom of this soft mud unit. Specific BBSS input provided in Table 7 does not list any sediment data for Layer 3. Attempts to model the actual data failed when using saturated sediment parameters. The matching response shown in Figure 14 was obtained by establishing the bottom boundary of the model at this interface and setting the reflection coefficient to  $-0.80$ . The large negative reflection coefficient indicates a decreasing impedance sequence and a drastic change in sediment type. Normally, this would be caused by gas bubbles trapped in the sediments. However, the fact that this area was most likely exposed pasture lands prior to flooding the reservoir, the acoustic response could indicate very low moisture content clays similar to hardpan. Either of these conditions could preclude one's ability to achieve sufficient penetration into these materials, particularly at 4-kHz. Also, this modeling technique is only valid in gas-free saturated sediments and could be a limiting factor at other sites regardless of seismic frequency.

**Site Ark14b.** This site is located approximately 200 ft past the end of the riprap blanket covering the toe of the dam (Figure 2 and Figure 23) along a short shelf that is possibly an engineered extension of the upstream face of the dam. These data indicate a more fully saturated sediment environment conducive to modeling hydroacoustic data. There are no measured subbottom reflectors in the vicinity of site Ark14b (Figure 2). Model comparison is presented in Figure 15 and the input parameters are listed in Table 8. The sediment models as a stiff clay/silt material with a porosity of 0.58, density of  $1.64 \text{ g/cm}^3$ , and reasonable frame bulk and shear moduli. The data are 'in-phase' with the source wavelet indicating a 'gas-free' environment. The core data (Appendix B) were taken in the vicinity of this site, i.e., near the toe of the dam, and show sands and clays with relatively low blow counts supporting the model predictions.

Table 7 Biot Model Geoacoustic Input Parameters; Site Ark14a					
	Layer 1	Layer 2	Layer 3	Layer 4	Layer 5
Label	Water	Soft Mud	Basement: Organic/ Unsaturated	Not Used	Not Used
Travel Time to bottom of layer, ms	9.13	9.98			
<b>Fluid</b>					
Fluid Density, g/cm <sup>3</sup>	1.0	1.0			
Fluid Bulk Modulus, dynes/cm <sup>2</sup> , xE+11	0.215	0.215			
Fluid Viscosity	0.019	0.019			
<b>Grain</b>					
Grain Density, dynes/cm <sup>2</sup>		2.53			
Grain Bulk Modulus (Real), xE+11		5.40			
Grain Shear Modulus (Real), xE+11		2.70			
Mean Grain Size, cm		0.0016			
<b>Frame</b>					
Porosity		0.84			
Permeability, cm/sec, xE-05		0.04			
Frame Bulk Modulus (Real), dynes/cm <sup>2</sup> , xE+09		No Frame			
Frame Bulk Modulus (Imag), dynes/cm <sup>2</sup> , xE+09		No Frame			
Frame Shear Modulus (Real), dynes/cm <sup>2</sup> , xE+09		No Frame			
Frame Shear Modulus (Imag), dynes/cm <sup>2</sup> , xE+09		No Frame			

Table 8 Biot Model Geoacoustic Input Parameters; Site Ark14b					
	Layer 1	Layer 2	Layer 3	Layer 4	Layer 5
Label	Water	Stiff Clay/Silt	Not Used	Not Used	Not Used
Travel Time to bottom of layer, ms	7.47	N/A			
<b>Fluid</b>					
Fluid Density, g/cm <sup>3</sup>	1.0	1.0			
Fluid Bulk Modulus, dynes/cm <sup>2</sup> , xE+11	0.215	0.215			
Fluid Viscosity	0.019	0.019			
<b>Grain</b>					
Grain Density, dynes/cm <sup>2</sup>		2.65			
Grain Bulk Modulus (Real), xE+11		5.40			
Grain Shear Modulus (Real), xE+11		2.70			
Mean Grain Size, cm		0.0016			
<b>Frame</b>					
Porosity		0.58			
Permeability, cm/sec, xE-05		0.003			
Frame Bulk Modulus (Real), dynes/cm <sup>2</sup> , xE+09		2.50			
Frame Bulk Modulus (Imag), dynes/cm <sup>2</sup> , xE+09		0.027			
Frame Shear Modulus (Real), dynes/cm <sup>2</sup> , xE+09		1.15			
Frame Shear Modulus (Imag), dynes/cm <sup>2</sup> , xE+09		0.037			

## Modeling summary

Three sites were modeled to describe general sediment conditions within Lake Arkabutla. Insufficient core data were available to intensively evaluate the BBSS program and to provide verification of predicted sediment types. Acoustic penetration was limited with the subbottom profiling systems used. Future survey programs should include a small sampling/coring program in conjunction with the geophysical surveys to calibrate and verify the analysis.

Given the limited ground truth data, the approach provided a method to rigorously interrogate actual sediment conditions from acoustic data. The Biot theory is a proven model. Acoustic calibration methods have been developed and employed here to quantify precisely the net acoustic response in a given sediment sequence. For data with sufficient signal response (Ark16a), the method provided reasonable estimates of sediment characteristics. The method also provided a critical evaluation of 'non-standard' sediment environments, such as site Ark14a, where it was not possible to match actual acoustic data using standard sediment parameter inputs.

## Inversion of Acoustic Data

Acoustic reflection data are processed through seismic inversion techniques to produce continuous sets of geopredicted sediment property values. This is accomplished through a software package developed by EHL, the BSED51 program, designed to incorporate calibrated acoustic data with modeled geoacoustic parameters. The BSED51 program was used to process all 4-kHz acoustic data. It provides graphics and digital sediment property output files and can be delivered as input data for all visualization and CADD work. Figure 16 shows density output graphic from the BSED51 program for the water-sediment interface along survey line 14 (Figure 2). Selected porosity ( $\beta$ ) and density ( $\rho$ ) values determined from the Biot calibration have been included for comparison with surface densities computed using BSED51. It shows excellent correlation between the modeled and processed results. The red dashed-line represents detected depth at the reflection interface used in the density calculations. Detection levels are controlled by the 'Threshold' variable and is analogous in function to the sensitivity control on a standard echosounding system. Processing input parameters are listed in the green control panel on the left side of the figure, and includes equipment calibration values (Table 4), detection threshold controls, transmitter/receiver geometry, and statistical processing controls. The geoacoustic calibration function, listed as 'Mobile Bay' in the control panel, is the impedance versus density model used for the Arkabutla Lake data. This relationship was derived during the geoacoustic-modeling phase of a previous survey performed in Mobile Bay, Alabama (McGee 1998). Acoustic response was similar to this survey in that a layer of unconsolidated fine sediments, or fluid mud, overlaid more competent native sediments. All 4-kHz data were processed through the BSED51 program to create matrices of position coordinates, depth, acoustic impedance, density, and porosity.

The BSED51 program was also used to conduct inversion on selected sub-bottom reflection interfaces. Accounting for two-way transmissivity and absorption through the upper layer the reflection coefficient and acoustic impedance can be calculated for subsequent deeper layers. The geoacoustic calibration function is the same as for the water-sediment interface. Figure 17 shows the graphical output screen from BSED51 along with selected BBSS reflection coefficient,  $R$ , value for model site Ark14a. Density spikes represent acoustic responses outside the boundaries established for a natural sediment response. Conditions at these locations seem to be unsaturated or consolidated clays and silts. The presence of interstitial gasses is also a possibility.

## 6 Data Presentation

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A brief description of physical conditions is provided to assess the spatial distribution of sediments within the surveyed portion of Lake Arkabutla. The purpose here is to present a range of possible data products available to assist in interpretations of geophysical survey data. A digital mosaic of side scan sonar imagery (Figure 11) was created to provide a contiguous picture of surficial sediment characteristics. Lakebed bathymetry data was compiled into a 20-ft by 20-ft resolution surface grid for contouring and as a base for overlays of specific sediment property information. Output from the BSED51 program was gridded for bulk density and sediment thickness to describe the actual sediment conditions. Figure 18 presents selected isometric views of sonar imagery, bathymetry, and sediment density with respect to water depth. This figure shows how this type information can be combined to provide enhanced interpretations of actual bottom conditions. For example, on the right side of Figure 18 is a small hard reflector (black contrast) near the front of the image. This corresponds to a small spike in the bathymetric data and a small high-density patch in the density image.

### Lakebed Sediment Density and Thickness

Surficial sediment density was continuously mapped over the extent of the survey area (Figures 18 and 19). Density is for the entire thickness of the upper sediment unit and shows a uniformly distributed layer of 1.2 - 1.4 g/cm<sup>3</sup> material. Density increases nearer the toe of the dam (western edge of map). Density is not reported for the riprap placed near the toe of the dam.

For Arkabutla, and other reservoirs, these data offer a complete picture of the distribution of sediments accumulating on the bottom of the lake. Combining physical property data such as density, with sediment thickness maps, it is possible to calculate the total volume of mud accumulated. Figure 20 presents a measured thickness for the upper sediment unit. This map was developed from the subbottom profile data by combining reflection interfaces from the digital subsurface model. Except for survey line 16 near the intake tower entrance, only a single subbottom interface at the bottom of the mud layer was detected. The data was not sufficient to develop more elaborate lithological models of Lake Arkabutla.

## Sediment Profiles

Six representative subbottom profile sections are presented in Figures 21 through 26. Each figure shows the actual subbottom profile data with the associated two-dimensional interpretations of lithology. This presentation is the basic 'fence diagram' format familiar to most geophysicists. The sediment units are grouped according to density range. After modeling, a basic sediment description was developed for each density range as presented in Table 5 (Chapter 5). Had there been confirming core sample data, more precise descriptions would have been developed, possibly relating to specific seismic issues. The profiles are self-explanatory and will only be briefly discussed following.

A 2- to 3-ft thick layer of soft mud overlays native soils along the eastern two-thirds of the survey area. No penetration was obtained through the native soils, resulting in a simple two-layer lithology. The western edge of the profiles extends over a riprap blanket along the toe of the dam. This zone of riprap is characterized by high-amplitude acoustic returns followed by numerous multiple reflections. Acoustic response in native soils tend to be high-amplitude with inconsistent wavelet polarity indicative of organic/gassy or unsaturated environments.

As shown by Figures 21 through 26, subbottom profiling allows for continuous surveys of subbottom conditions from which an optimum sediment sampling/coring plan can be developed assuring sampling from all sediment units. Through geoacoustic modeling of the sediment and acoustic data, physical properties can be determined for all survey data providing accurate data over large geographic areas. This would reduce or even eliminate the potential of erroneous extrapolation of sediment conditions between isolated core locations.

## 7 Conclusions and Recommendations

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Prior to the filling of Lake Arkabutla, the area upstream of the dam was comprised of agricultural lands. The only sediments to be found were those deposited within the banks of the streams meandering through the watershed. Except for the relic streambed, the former surface soils act as the confining acoustic interface (Figure 2), limiting penetration to the bottom of the layer of sediments accumulated since filling of the reservoir. Within the meandering streambed, nearly 17 ft of acoustic penetration was achieved for the 1- to 4-kHz frequency bandwidth chosen. In these areas, sediment characterization was reasonable as shown by Figures 1, 13 and 24.

The instruments selected for this initial investigation were not adequate due to frequency and source level to overcome attenuation caused by the confining layer. This confining layer is likely comprised of compacted, unsaturated soils possibly containing decomposing organics found over most of the project site. This may be a typical configuration for man-made reservoirs. For an acoustic solution, a lower frequency system is recommended.

Specific conclusions and recommendations for the Lake Arkabutla sediment characterization feasibility study are provided following.

### Conclusions

#### Biot theory

The Biot theory is a proven method (see references). For Arkabutla survey data with sufficient signal response, the method provided, in the absence of quantified ground truth from the core data, reasonable estimates of sediment density, porosity, acoustic wave speed and attenuation were obtained.

The method of forward modeling to develop site specific transfer functions relating acoustic response to sediment properties provided a critical evaluation of the sediment environment at Lake Arkabutla. This allowed for analysis of 'non-standard' sediment configurations.

Sediment bulk density, computed from acoustic impedance, is considered the most reliable sediment parameter for Arkabutla and best represents in situ conditions.

### **Core sampling**

No sampling or coring was conducted in conjunction with this investigation. Core data retrieved from near the upstream toe of the dam (Appendix B) was provided from a previous investigation (reference if needed).

No laboratory measurement of any of the thirteen physical Biot parameters was available from the existing core data. This provided only general guidance from which the Biot theory could be used in a predictive mode.

Core positioning was not coordinated in conjunction with the geophysical survey nor was it possible to accurately determine their precise location.

### **Acoustic response**

Characterization of sediments accumulated since filling of the reservoir was accomplished in terms of density and sediment thickness providing information useful in accurately determining the rate and composition of sedimentation in Lake Arkabutla. The data were collected rapidly and continuously, providing full coverage mapping of sediment conditions within the lake.

Information regarding the reflection coefficient for the water-sediment interface, attenuation through the upper sediment layer, and reflectivity of the confining layer was obtained.

Within the former riverbed, acoustic penetration and signal response was sufficient to characterize sediment conditions down to nearly 17 ft below the lake bottom using the 1- and 4-kHz systems.

An acoustically confining layer of compacted unsaturated soils limited acoustic penetration to the bottom of the sediment layer. This layer did not respond acoustically as a standard sediment. Both the 1-kHz and 4-kHz systems were unable to penetrate through this native soil unit.

## **Recommendations**

A follow-on field study with an acoustic source operating in the seismic range, i.e., 100-500-Hz should be conducted to fully evaluate the feasibility of an acoustics approach. This would likely involve use of a small airgun source.

A ground penetrating radar (GPR) system should be included as part of the field investigation to verify the presence of acoustic-inhibiting conditions such as decomposing organics.



A coring program resulting from the geophysical investigation is recommended. Core locations should be selected based on survey results. If good core data already exists, the geophysical survey must be designed to collect acoustic information precisely over the core location.

Cores should be analyzed for density, porosity, sound velocity, and specific gravity along with a complete grain size analysis. This will provide sufficient information for calibration of geoacoustic conditions using the Biot theory.

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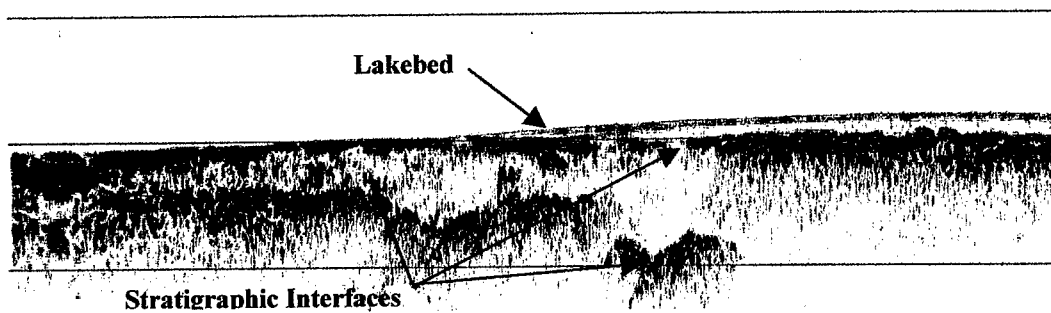


Figure 1. Example subbottom profile from Lake Arkabutla

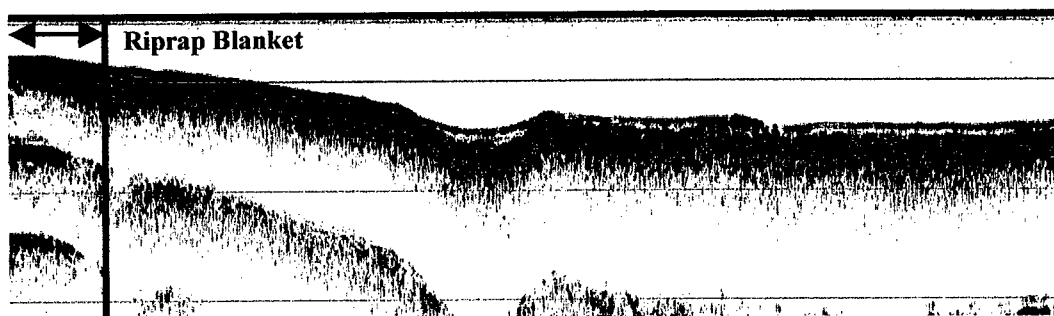


Figure 2. Typical subbottom profile data from Lake Arkabutla

# GEOACOUSTIC MODELLING

Reflection Coeff  
Impedance  
Velocity  
Absorption  
Phase

Interstitial Fluid  
Sediment Grains  
Sediment Frame

**BIOT**  
**MECH**

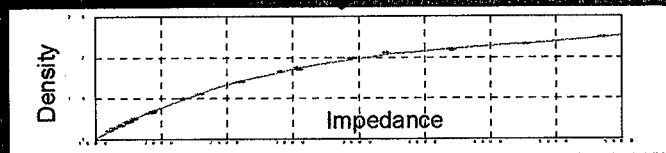
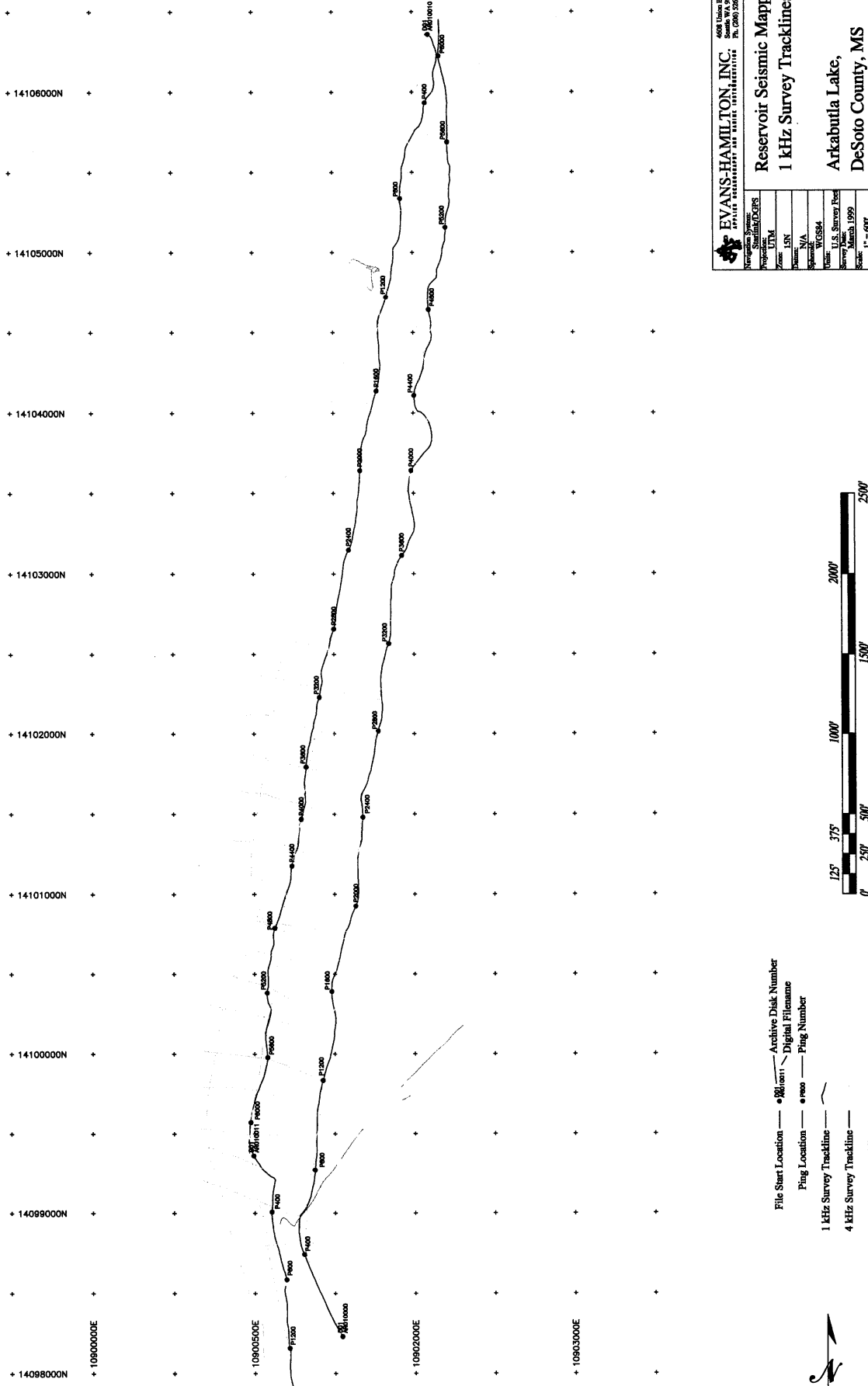
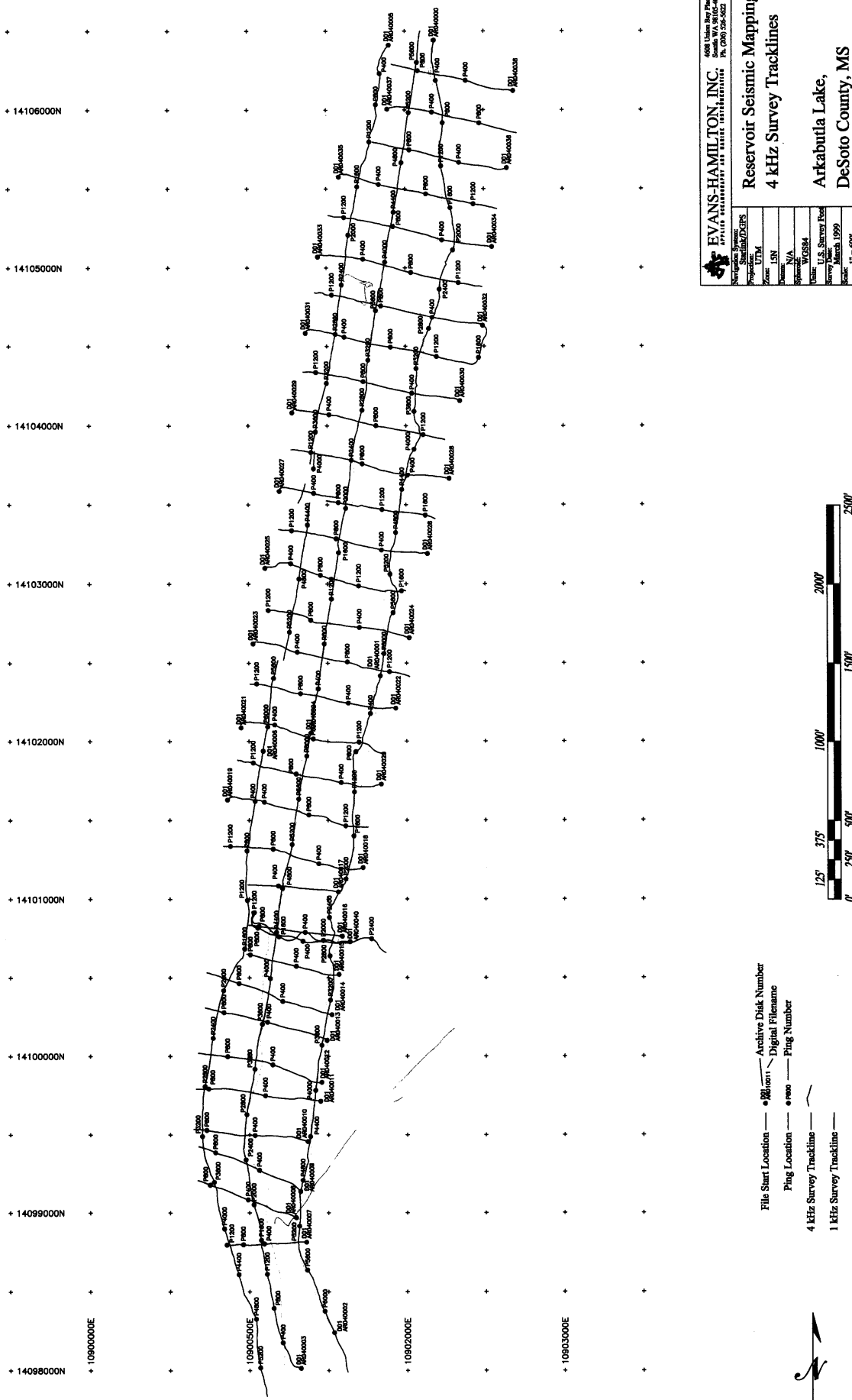



Figure 3. Biot-based modeling concept



<b>EVANS-HAMILTON, INC.</b> 4000 N. Highway 100, Suite 100 South WA 99155-0024 Ph. (509) 236-5822	
Project:	Reservoir Seismic Mapping
Product:	1 kHz Survey Tracklines
Client:	Arkabutla Lake, DeSoto County, MS
Zone:	UTM
Datum:	USNA
Projection:	WGS84
Units:	U.S. Survey Feet
Survey Dates:	March 1999
Scale:	1" = 600'
Surveyed By:	Richard McCree
Checked By:	Richard McCree
Drawn By:	Richard McCree
Project No.:	4700.39
Sheet No.:	

Figure 4. Lake Arkabutla 1-kHz survey track lines.




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**Reservoir Seismic Mapping**  
**4 kHz Survey Tracklines**  
  
**Arkabutla Lake,**  
**DeSoto County, MS**

Project	Arkabutla Lake	Client	U.S. Army Corps of Engineers
Zone	UTM	Scale	1" = 600'
U.S. Survey Foot	March 1999	Surveyed By	Richard McGee
Surveyed	March 1999	Drawn By	Richard McGee
Scale	1" = 600'	Checked By	Richard McGee
Surveyed	March 1999	Sheet No.	
Drawn	March 1999	Sheet No.	
Checked	March 1999	Sheet No.	
Surveyed	March 1999	Sheet No.	

- File Start Location — ●
- Archive Disk Number — ●
- Digital Filename — ●
- Ping Location — ●
- Ping Number — ●
- 4 kHz Survey Trackline — —
- 1 kHz Survey Trackline — —
- Survey Calibration Trackline — —

Figure 5. Lake Arkabutla 4-kHz survey track lines.



Figure 6. Survey vessel *Nancy Kay* at Lake Arkabutla

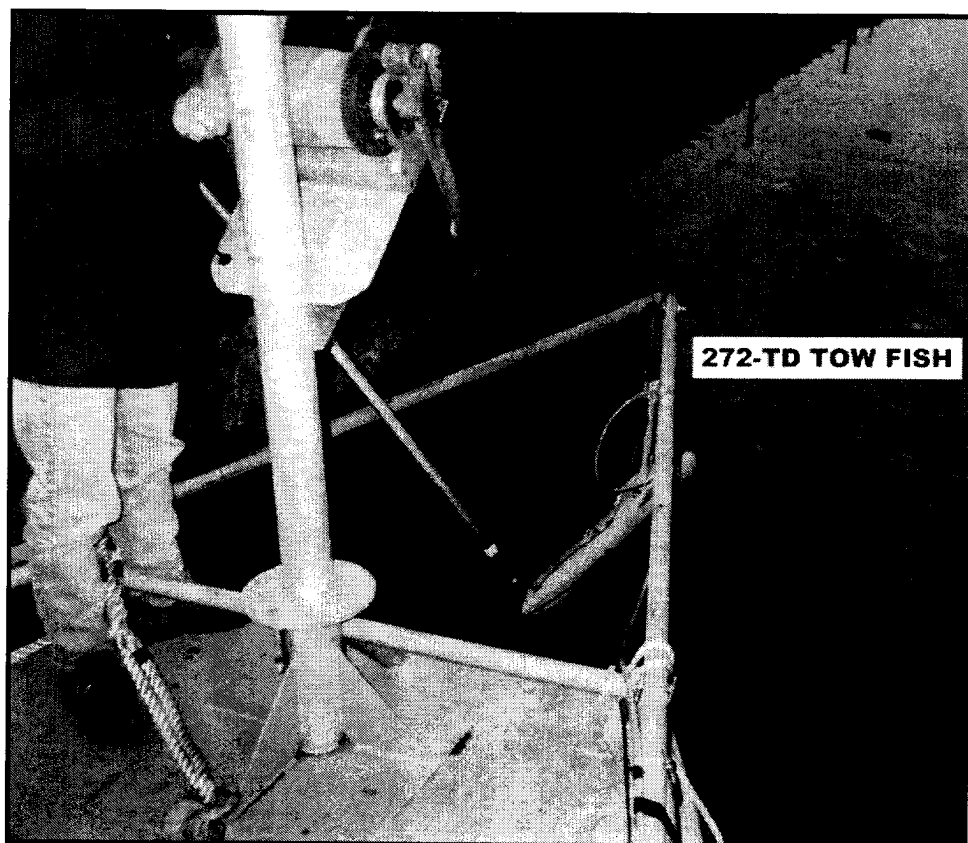


Figure 7. Side scan tow fish deployed over bow of *Nancy Kay*

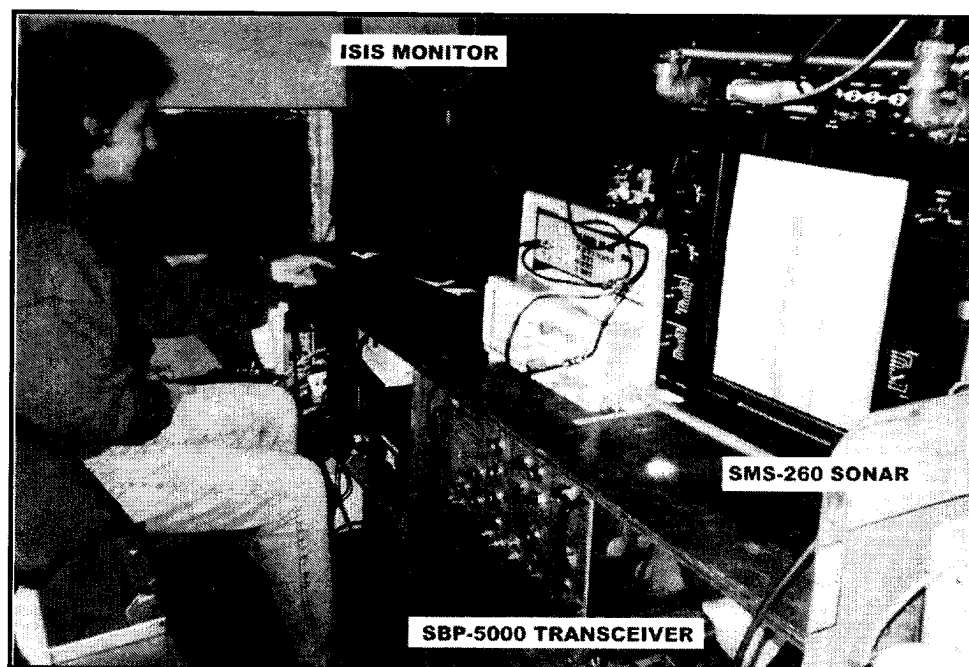


Figure 8. Geophysical data acquisition



4 kHz

Top of Mud

Native Material

Multiple

1 kHz

Top of Mud

Native Material

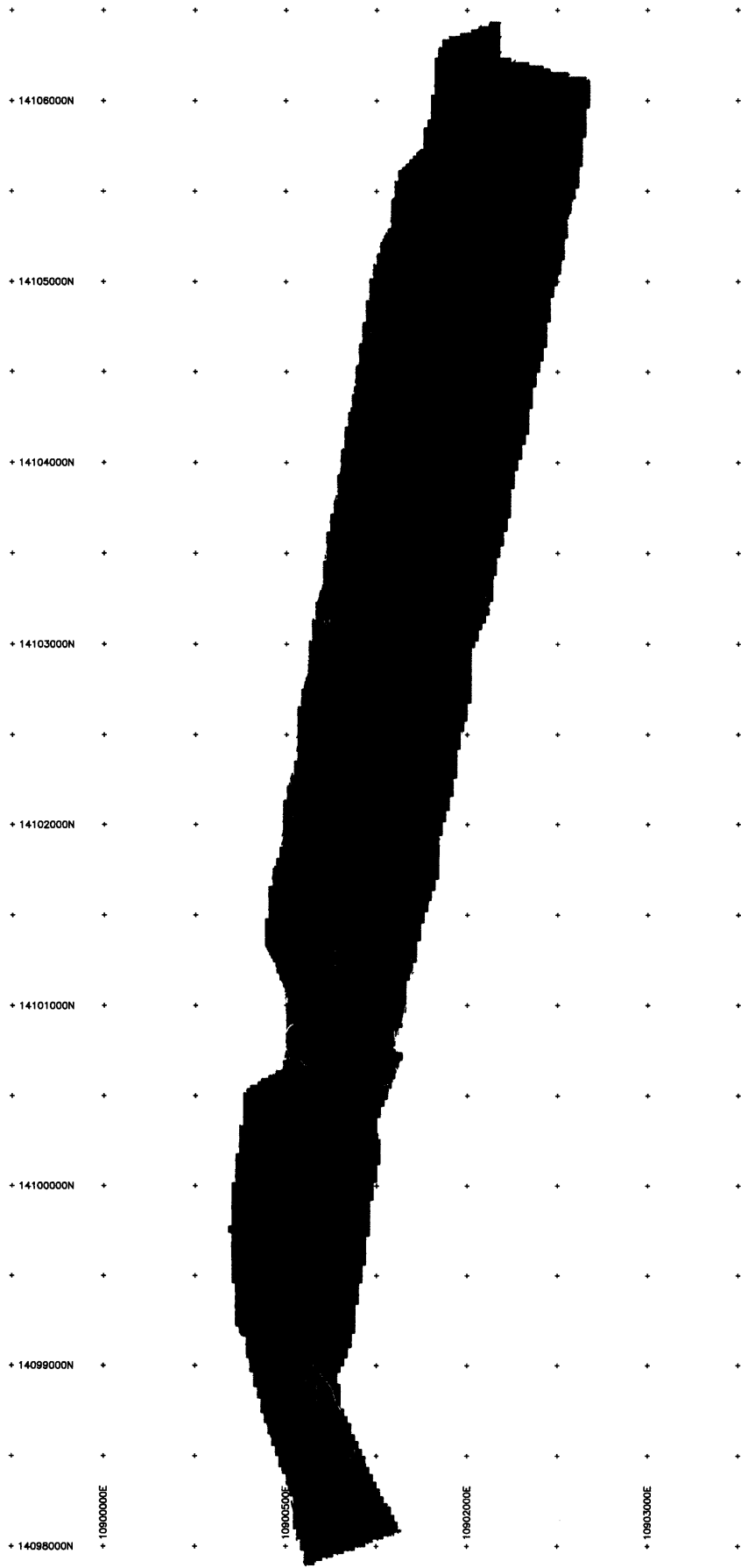
Multiple

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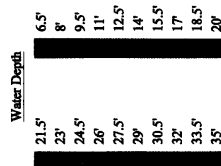
**Reservoir Seismic Mapping**  
**Comparison of 1 kHz and**  
**4 kHz Subbottom Profiles**  
**Arkabutla Lake,**  
**DeSoto County, MS**

Navigation System	StarLine/DOCS	Project	Arkabutla Lake
Projection	UTM	Date	June 1999
Zone	18N	Sheet Edition No.	1
Datum	NAD 83	Plan No.	
Scale	1:50,000	Sheet No.	
U.S. Survey Foot	1:50,000	Drawn by	Richard McCreary / Brent Johnson
Survey Date	June 1999	Checked by	Richard McCreary
Scale	1:50,000		

Figure 9. 1- and 4-kHz subbottom profile comparison.

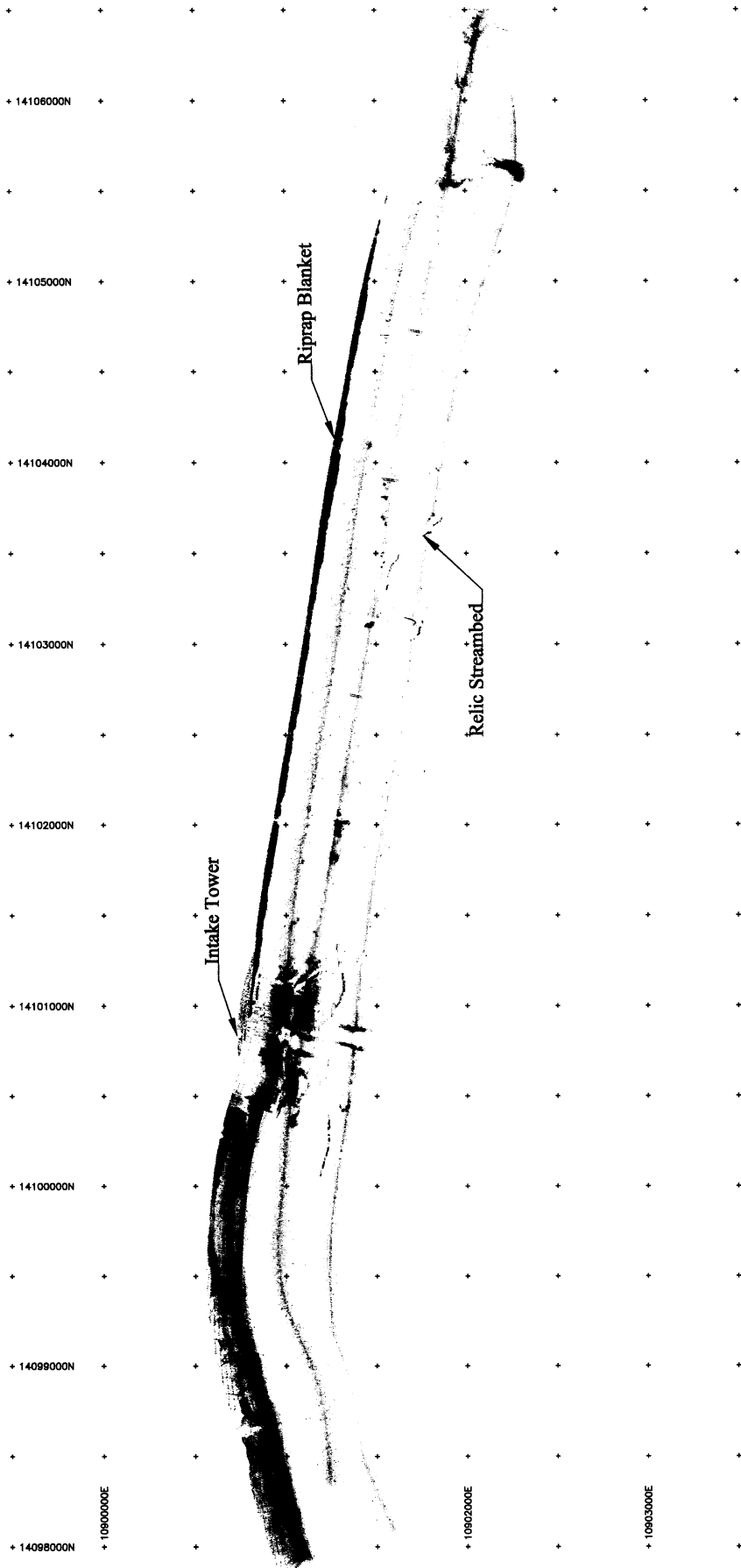


One Foot Contour Interval



<b>EVANS-HAMILTON, INC.</b> <small>4088 Union Bay Place N.E.          Suite 100, Jacksonville, FL 32216          Phone: (904) 226-5822</small>	
<b>Reservoir Seismic Mapping</b> <b>Lakebed Bathymetry</b>	<b>Arkabutla Lake,</b> <b>DeSoto County, MS</b>
<b>Navigation System:</b> Starlink/DGPS <b>Projection:</b> UTM <b>Zone:</b> 18N <b>Datum:</b> NAD83 <b>Ellipsoid:</b> GRS80 <b>Units:</b> U.S. Survey Feet <b>Survey Date:</b> March 1999 <b>Scale:</b> 1" = 600' <b>Surveyed By:</b> Richard McGee <b>Drawn By:</b> John Rodman / Brent Johnston <b>Checked By:</b> Richard McGee	<b>Reference:</b> Date: June 1999 Job No.: 0700.39 Sheet Reference No.: Sheet No.:

Figure 10. Bathymetry map, Lake Arkabutla.



Note: Misalignments between sonar swaths due to poor quality DGPS signal during time of survey. No attempt was made during processing to adjust.



<b>EVANS-HAMILTON, INC.</b> 4401 N. Hwy. 112, Box 112 South, WA 99155-0012 Ph. (509) 256-5822		Navigation System: Garmin 100/DGPS	
Projection:	UTM	Zone:	18N
Datum:	USN	Datum:	NAD83
Units:	US Survey Feet	Scale:	1" = 400'
Survey Name:	March 1999	Surveyed By:	Richard McKee
Survey Date:	March 1999	Processed By:	Richard McKee
Surveyed By:	Richard McKee	Checked By:	Richard McKee
Drawn By:	Richard McKee	Scale No.:	
Client:	Arkabutla Lake, DeSoto County, MS	Sheet No.:	

Figure 11. Side scan sonar mosaic, Lake Arkabutla.

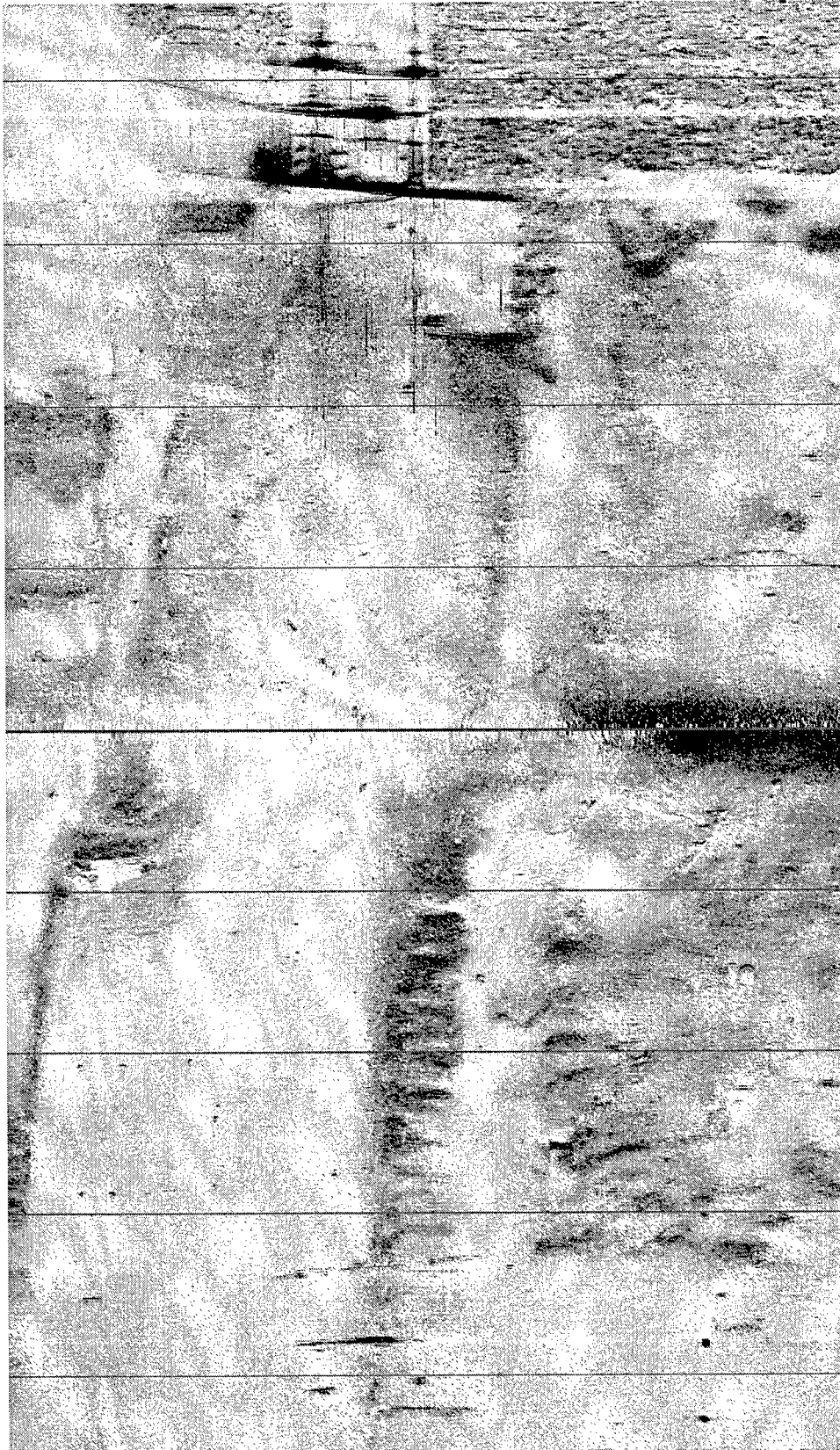


Figure 12. Side scan image of approach to intake

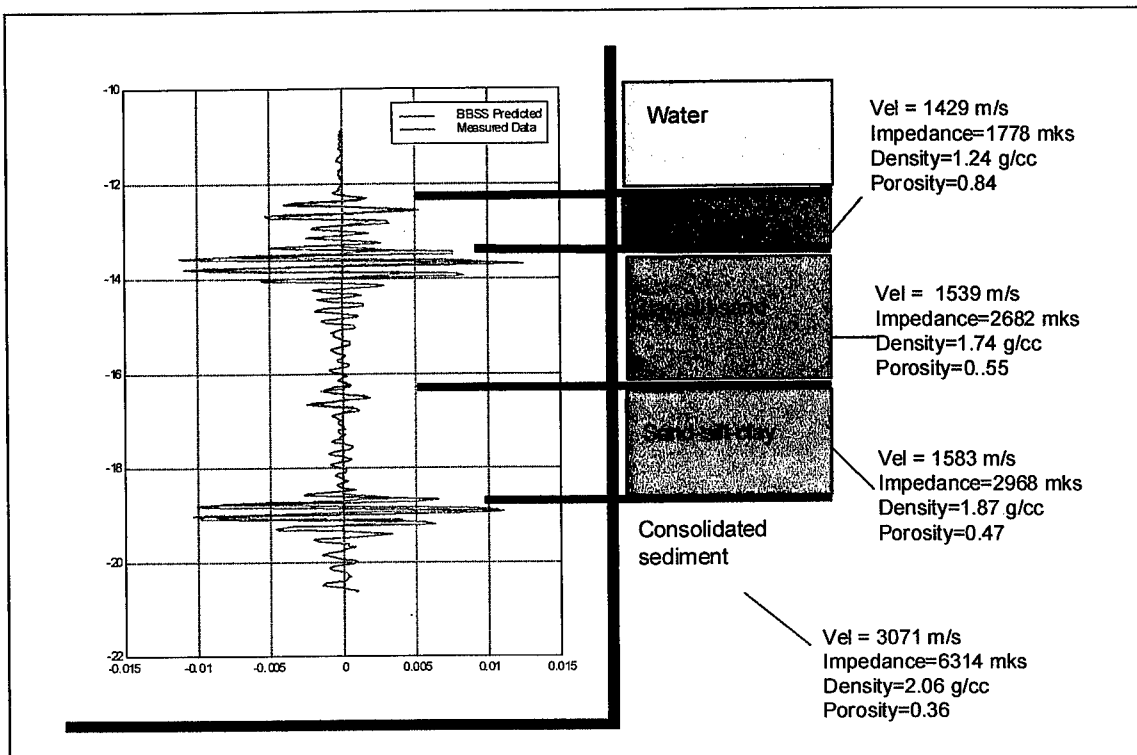


Figure 13. Geoacoustic model; Site Ark16a

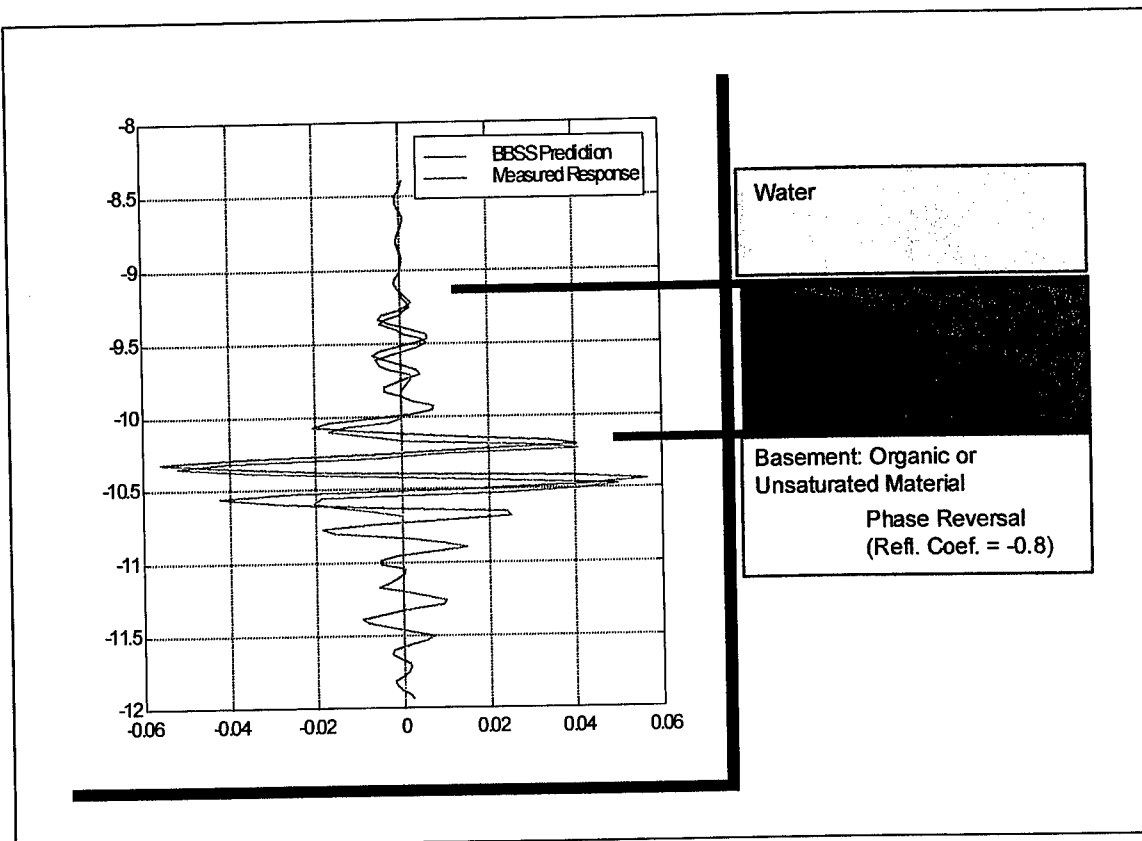


Figure 14. Geoacoustic model; Site Ark14a

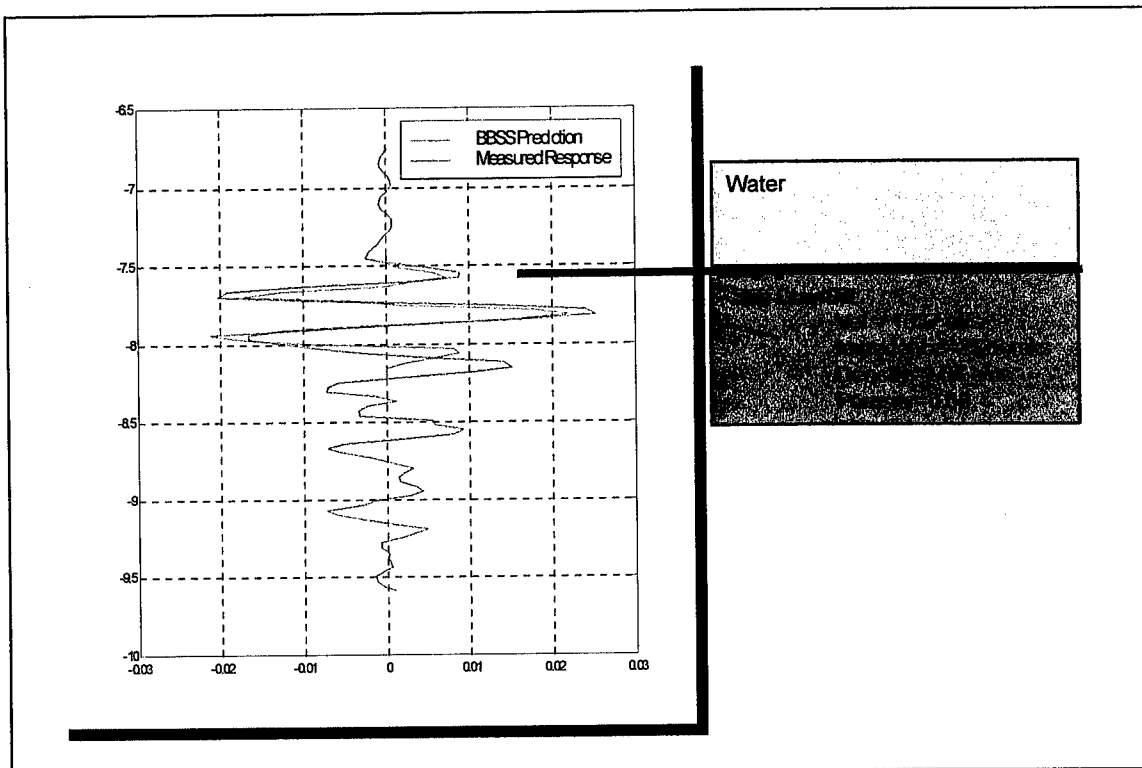


Figure 15. Geoacoustic model: Site Ark14b

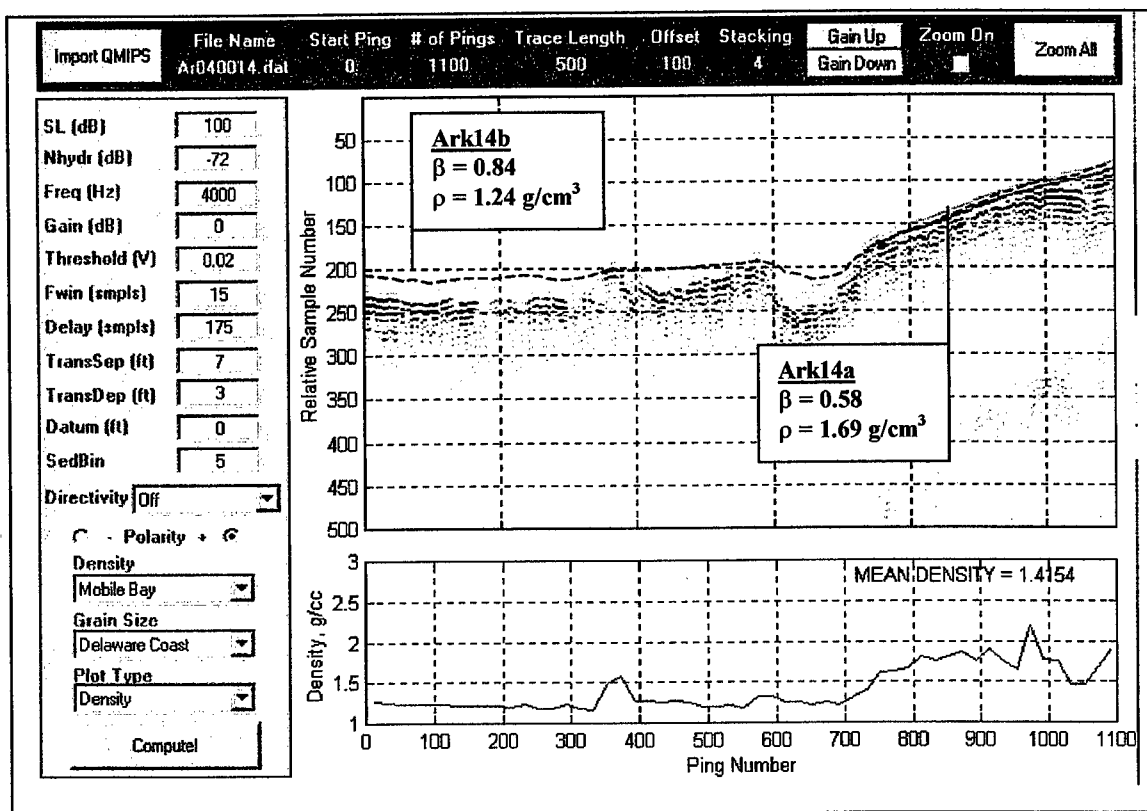


Figure 16. BSED51 output at water-sediment interface



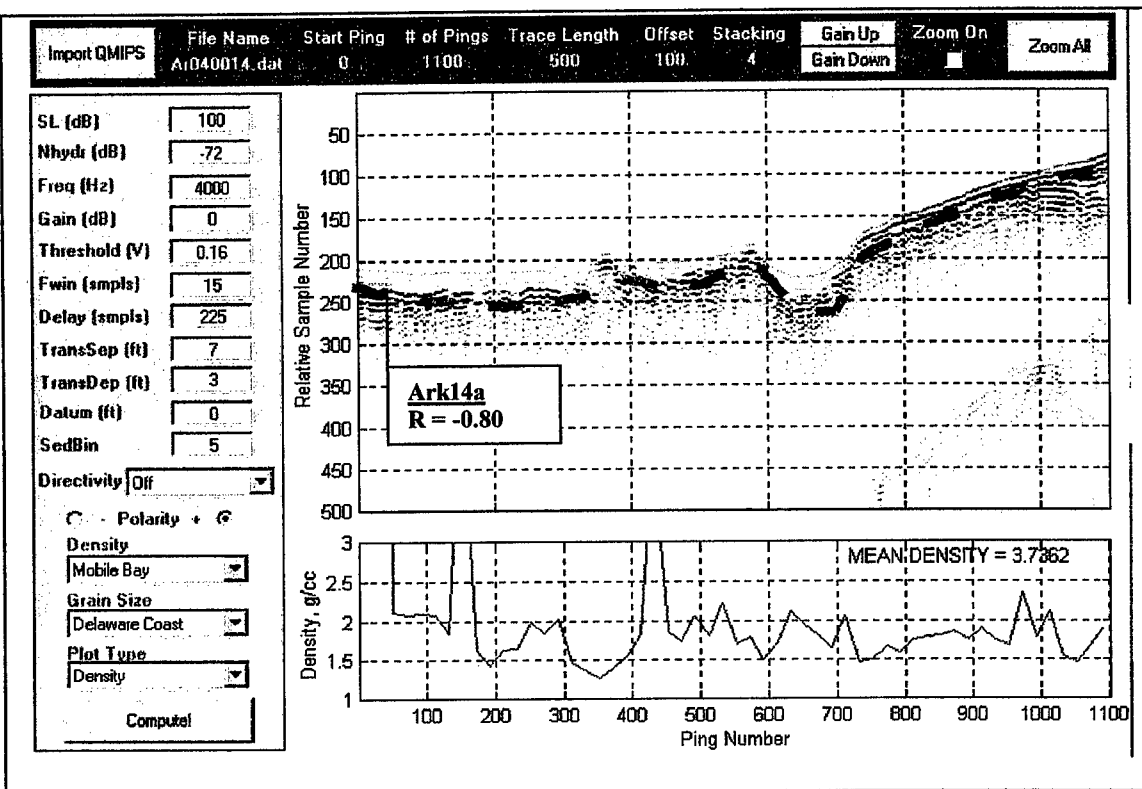
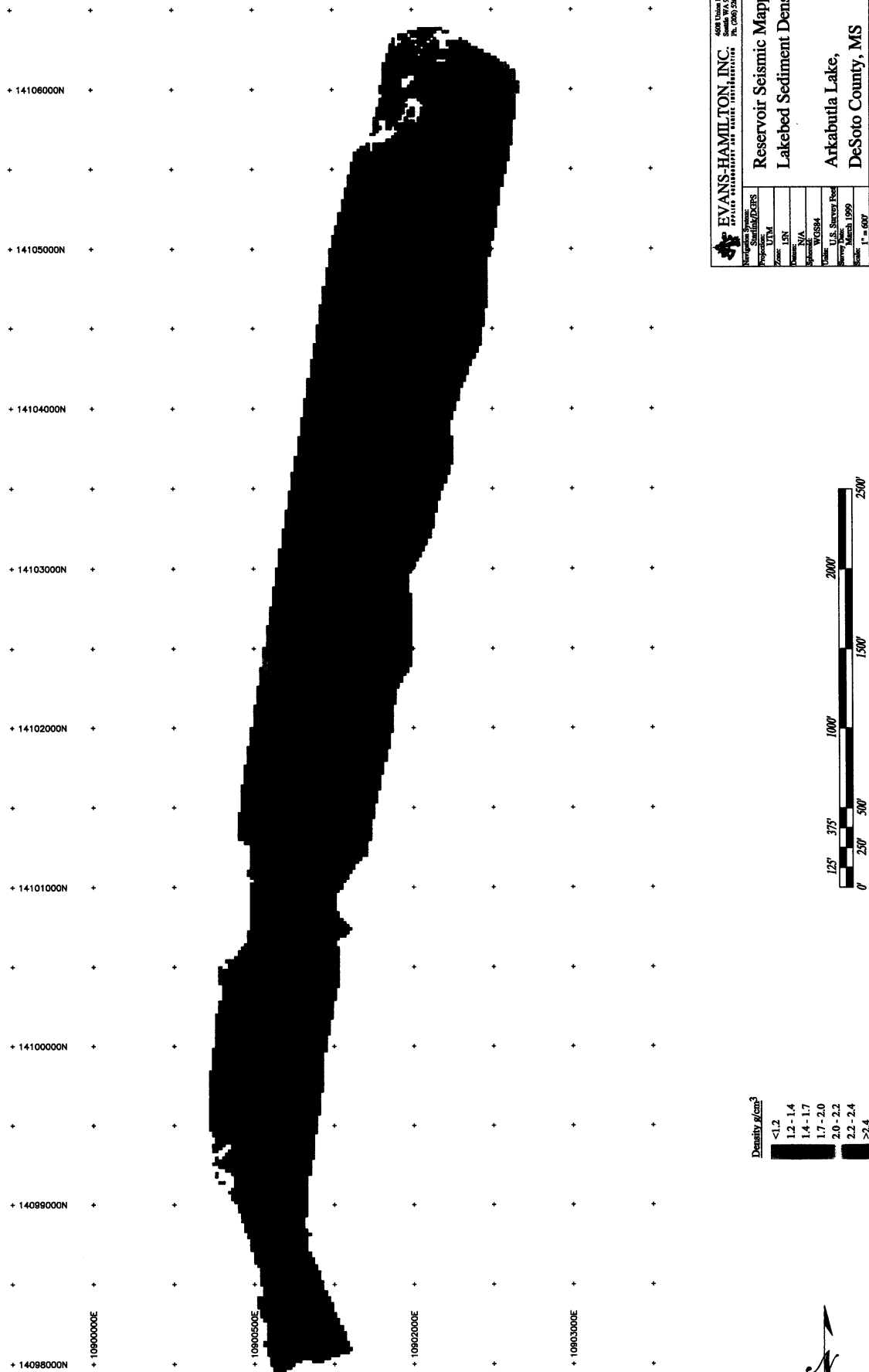


Figure 17. BSED51 output at data basement





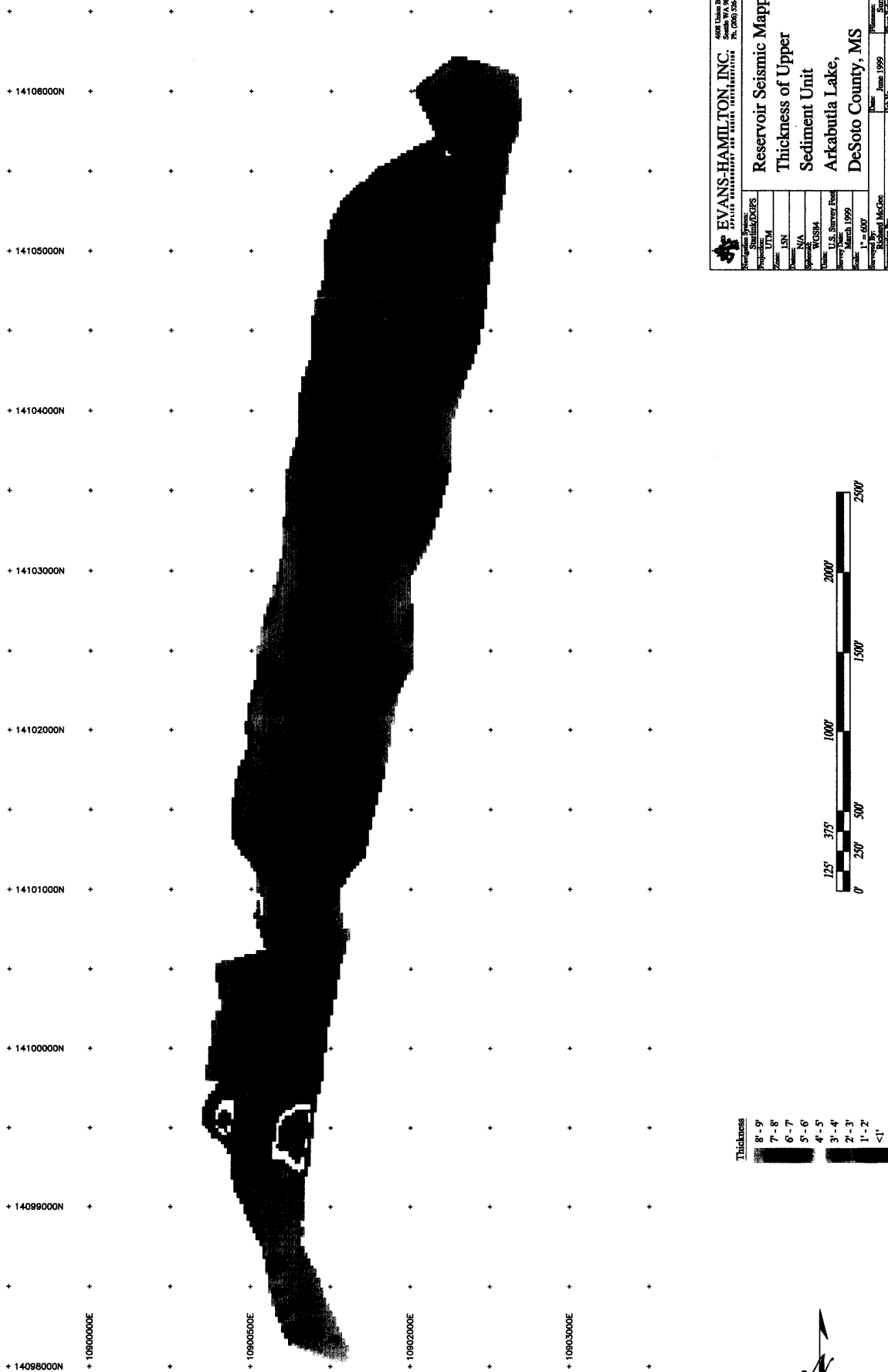
**EVANS-HAMILTON, INC.**  
608 Union Bay Place N.E.  
Atlanta, Georgia 30308  
Phone: (404) 256-5522

**Navigation System:** Surface/DGPS  
**Projection:** UTM  
**Zone:** 18N  
**Datum:** NAD83  
**Units:** Meters  
**Scale:** 1" = 400'  
**UTM:** U.S. Survey Feet  
**Survey Date:** March 1999  
**Scale:** 1" = 400'

**Reservoir Seismic Mapping**  
**Lakebed Sediment Density**  
**Arkabutla Lake,**  
**DeSoto County, MS**

Survey	Date	Project	Sheet
Survey	March 1999	Arkabutla Lake	Sheet 1 of 1
Drawn By:	Richard I. McGee	Checked By:	Richard I. McGee
Drawn By:	Richard I. McGee	Checked By:	Richard I. McGee

Figure 19. Surficial sediment density distribution.



<b>EVANS-HAMILTON, INC.</b> <small>6081 Tulsa Bay Place N.E.          Oklahoma City, Oklahoma 73106-3602          PH. (405) 256-5622</small>		<b>Reservoir Seismic Mapping</b> <b>Thickness of Upper</b> <b>Sediment Unit</b> <b>Arkabutla Lake,</b> <b>DeSoto County, MS</b>	
Navigation System	Survey Method	Date	Release
Geomatics/DOCS	UTM	June 1999	SurfPlan.dwg
Zone: 18N	UTM	483	Sheet Name: No.
Datum: NAD83	UTM	4700.39	Sheet No.
Projection: UTM	UTM		Sheet No.
Scale: 1" = 600'	UTM		Sheet No.
Survey Method: U.S. Survey Feet	UTM		Sheet No.
Survey Date: March 1999	UTM		Sheet No.
Surveyed By: Richard McCoy	UTM		Sheet No.
Checked By: Richard McCoy / Brent Johnston	UTM		Sheet No.
	UTM		Sheet No.

Figure 20. Thickness isopach of upper sediment unit.

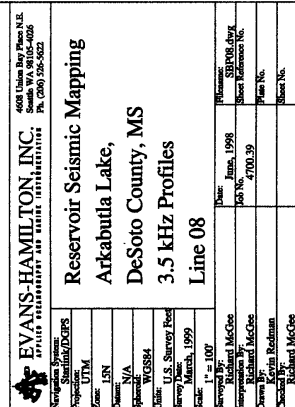
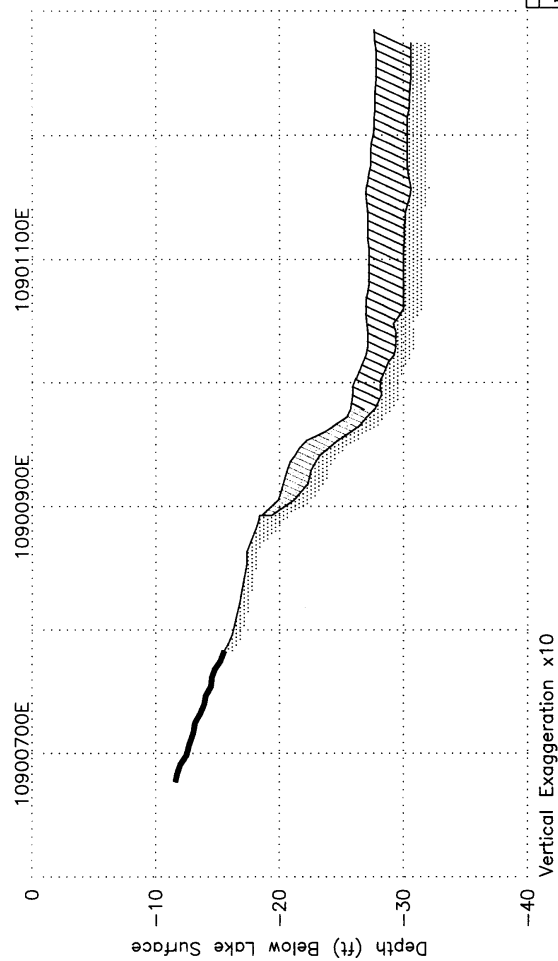
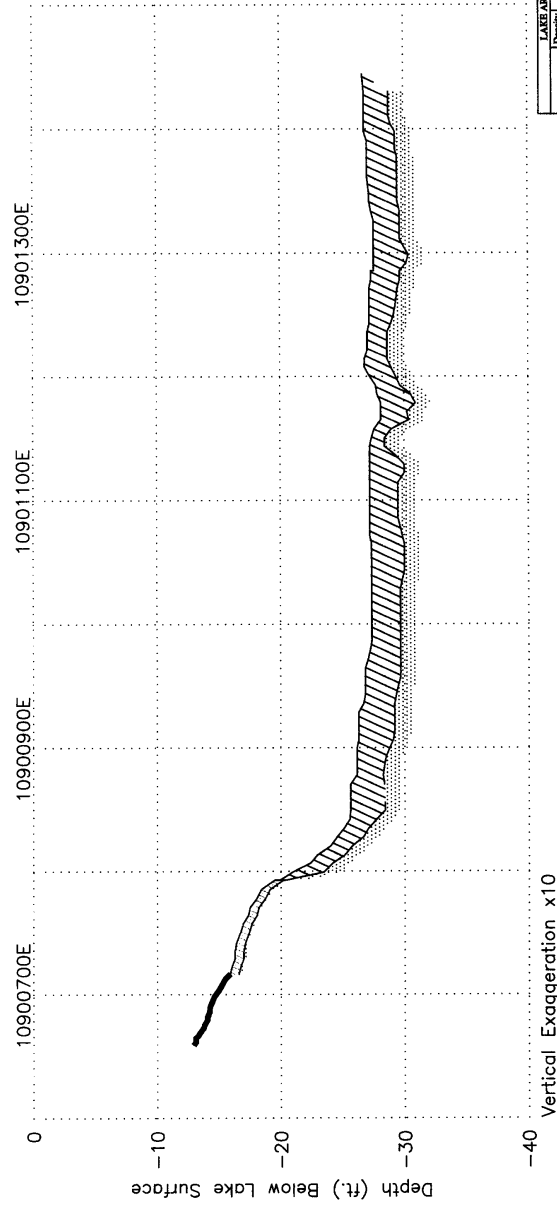
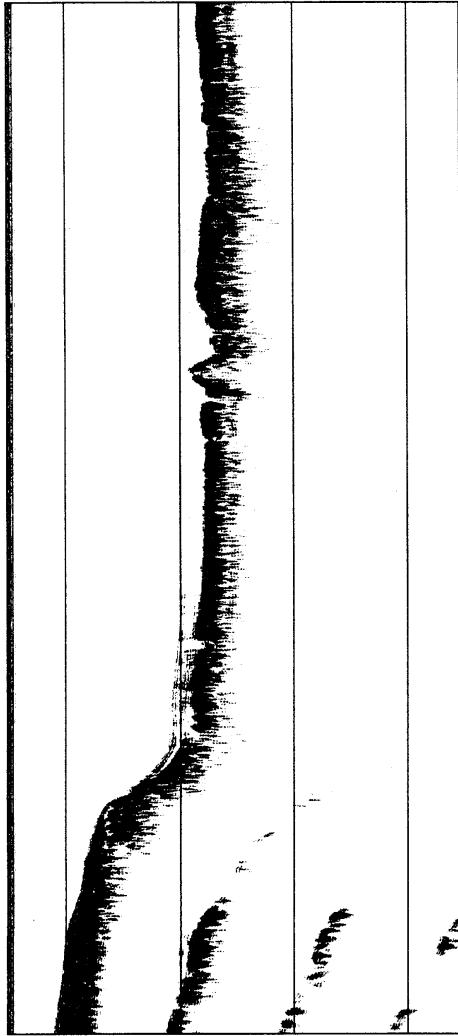


Figure 21. Sediment profile, Line 08.



Vertical Exaggeration x10

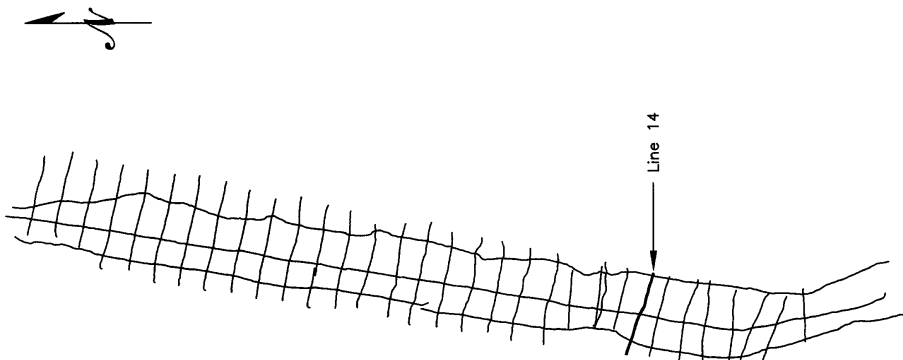
LAKE ARKABUTLA SEDIMENT DESCRIPTION	
Symbol	Density g/cm <sup>3</sup>
Blank	< 1.2
Diagonal lines	1.2 - 1.4
Horizontal lines	1.4 - 1.7
Vertical lines	1.7 - 2.0
Stippled	2.0 - 2.2
Blank	N/A


LAKE ARKABUTLA SEDIMENT DESCRIPTION	
Symbol	Density g/cm <sup>3</sup>
Blank	< 1.2
Diagonal lines	1.2 - 1.4
Horizontal lines	1.4 - 1.7
Vertical lines	1.7 - 2.0
Stippled	2.0 - 2.2
Blank	N/A

LAKE ARKABUTLA SEDIMENT DESCRIPTION	
Symbol	Density g/cm <sup>3</sup>
Blank	< 1.2
Diagonal lines	1.2 - 1.4
Horizontal lines	1.4 - 1.7
Vertical lines	1.7 - 2.0
Stippled	2.0 - 2.2
Blank	N/A

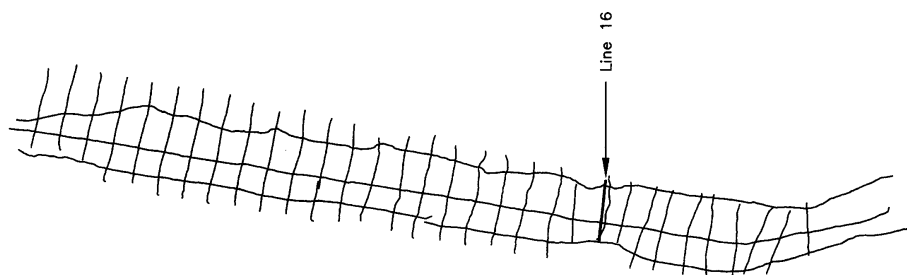
<b>EVANS-HAMILTON, INC.</b> 408 Lake Bay Pkwy N.E. South WA 98105-4026 PH (206) 256-5622	
<b>Reservoir Seismic Mapping</b> Arkabutla Lake, DeSoto County, MS 3.5 kHz Profiles Line 11	
Project: Date: Zone: Scale: 1" = 100' Surveyed by: Date: Sheet No.: Sheet Range:	Project: Date: Zone: Scale: 1" = 100' Surveyed by: Date: Sheet No.: Sheet Range:
Project: Date: Zone: Scale: 1" = 100' Surveyed by: Date: Sheet No.: Sheet Range:	Project: Date: Zone: Scale: 1" = 100' Surveyed by: Date: Sheet No.: Sheet Range:


Figure 22. Sediment profile, Line 11.



 <b>EVANS-HAMILTON, INC.</b> SPECIAL DEVELOPMENT AND TESTING INSTRUMENTATION 4608 North Bay Plaza, N.E. Seattle, WA 98105-4028 PH. (206) 726-8822	<b>Reservoir Seismic Mapping</b> <b>Arkabutla Lake,</b> <b>DeSoto County, MS</b> <b>3.5 kHz Profiles</b> <b>Line 14</b>		<b>Name</b> James, 1998 <b>MS No.</b> 4700.39 <b>Date No.</b> <b>Sheet No.</b>
	<b>Version</b> Final <b>Project</b> Arkabutla Lake Seismic Profiles <b>Date</b> UTM <b>Zone</b> 18N <b>Name</b> N/A <b>Number</b> 0384 <b>Name</b> U.S. Survey Post <b>Date</b> March, 1999	<b>Interval =</b> 1' 00" <b>Surveyed by</b> Richard McCoe <b>Processed by</b> Keris Redman <b>Edited by</b> Richard McCoe	<b>Project</b> EBP14 Line 14 <b>Sheet Reference No.</b> <b>Date No.</b> <b>Sheet No.</b>

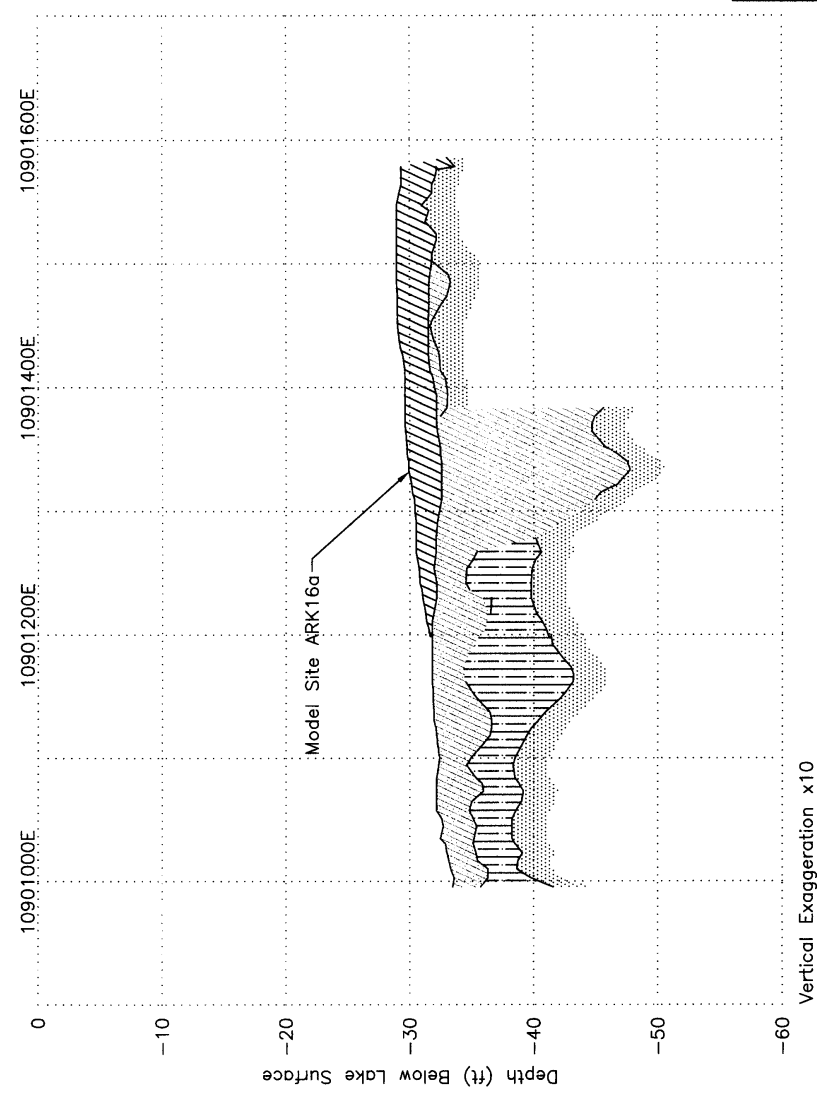
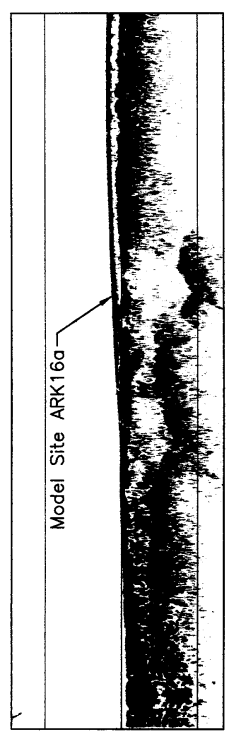
Filename:	SBP14.dwg
Sheet Reference No.	
Plate No.	
Sheet No.	



**EVANS-HAMILTON, INC.**  
400 Union Gap Road, N.E.  
Snohomish, WA 98066-4005  
PH: (360) 525-5022

**Reservoir Seismic Mapping**  
Arkabutla Lake,  
DeSoto County, MS  
3.5 kHz Profiles  
Line 16

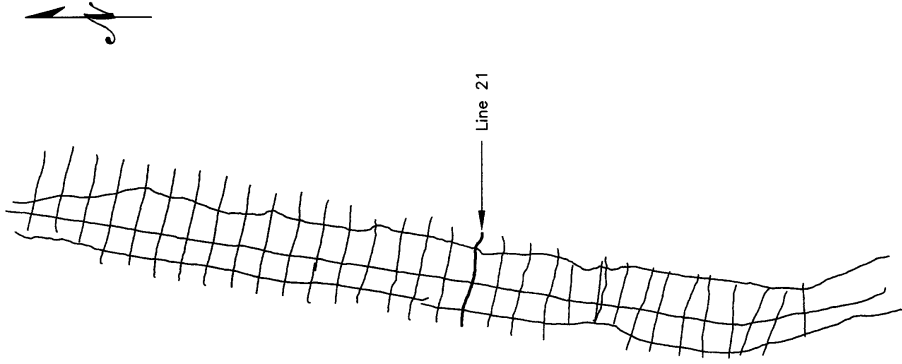
Project Name	Arkabutla Lake Seismic Mapping
Client	U.S. Army Corps of Engineers
Location	Arkabutla Lake, DeSoto County, MS
Scale	1" = 100'
Survey Date	March, 1999
Surveyed By	Richard McGee
Checked By	Richard McGee
Drawn By	Richard McGee
Job No.	1700.39
Plan No.	
Sheet No.	



LAKES ARKABUTLA SEDIMENT DESCRIPTION	
Hand Pattern	Density
	g/cm <sup>3</sup>
	< 1.2
	1.2 - 1.4
	1.4 - 1.7
	1.7 - 2.0
	2.0 - 2.2
	N/A
Sediment Description	
Basic Sediment Description	
Field Note: Flat	
Unconsolidated Med. Saturated Clay, Sil	
Clay-Silt, Clay-Silt-Sand Mixture	
Soft Clayey Sand, Silty Sand, Fine Sand	
Dense Clay, Unconsolidated Sediment, Possible Organic	
Riprap Blanket	

Figure 24. Sediment profile, Line 16.

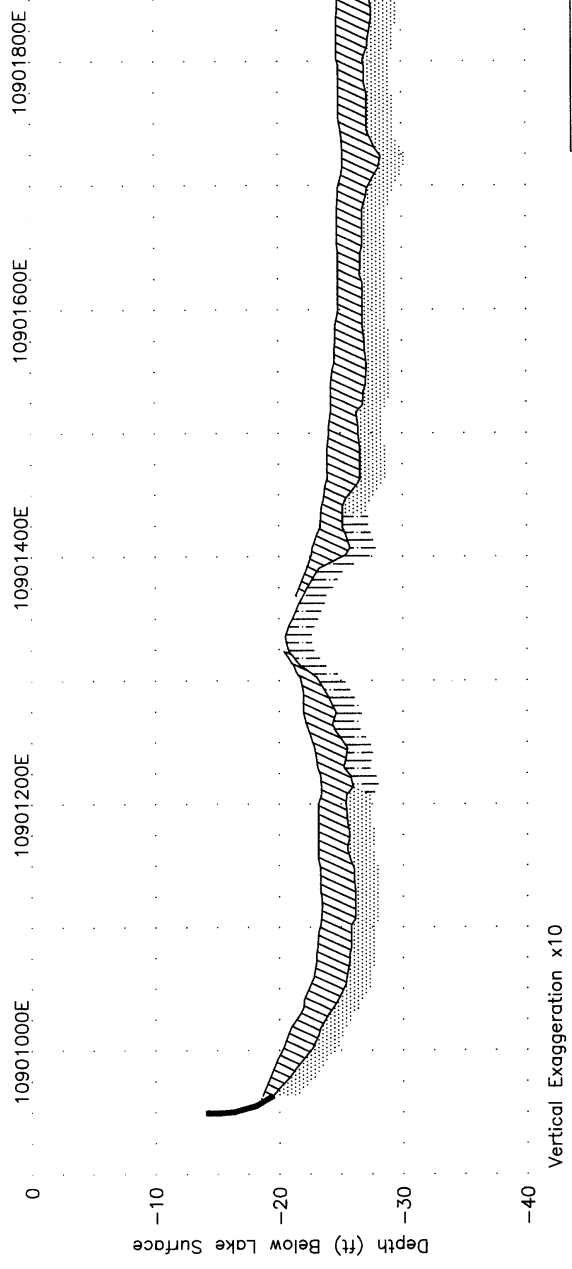




**EVANS-HAMILTON, INC.**  
 4000 Union Way, Suite 112  
 South WA 99124-4005  
 PH: (509) 256-5022

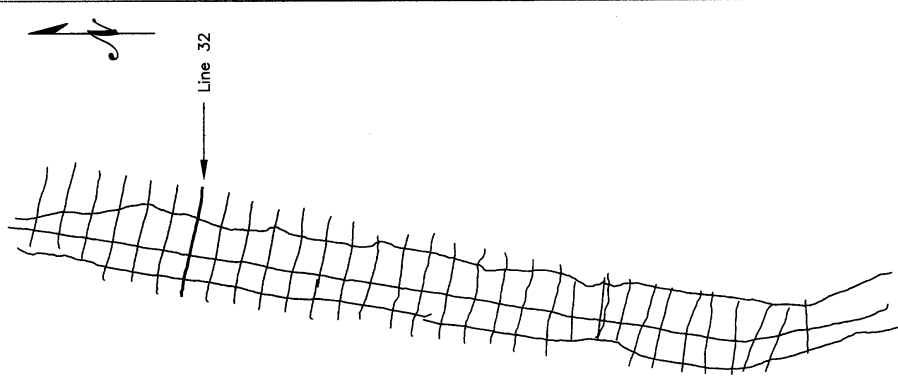
**Reservoir Seismic Mapping**  
**Arkabutla Lake,**  
**DeSoto County, MS**  
**3.5 kHz Profile**  
**Line 21**

Project: Arkabutla Lake  
 Date: June, 1999  
 Scale: 1" = 100'  
 Drawn By: Richard McCoe  
 Checked By: Richard McCoe  
 Sheet No.:



Vertical Exaggeration x10

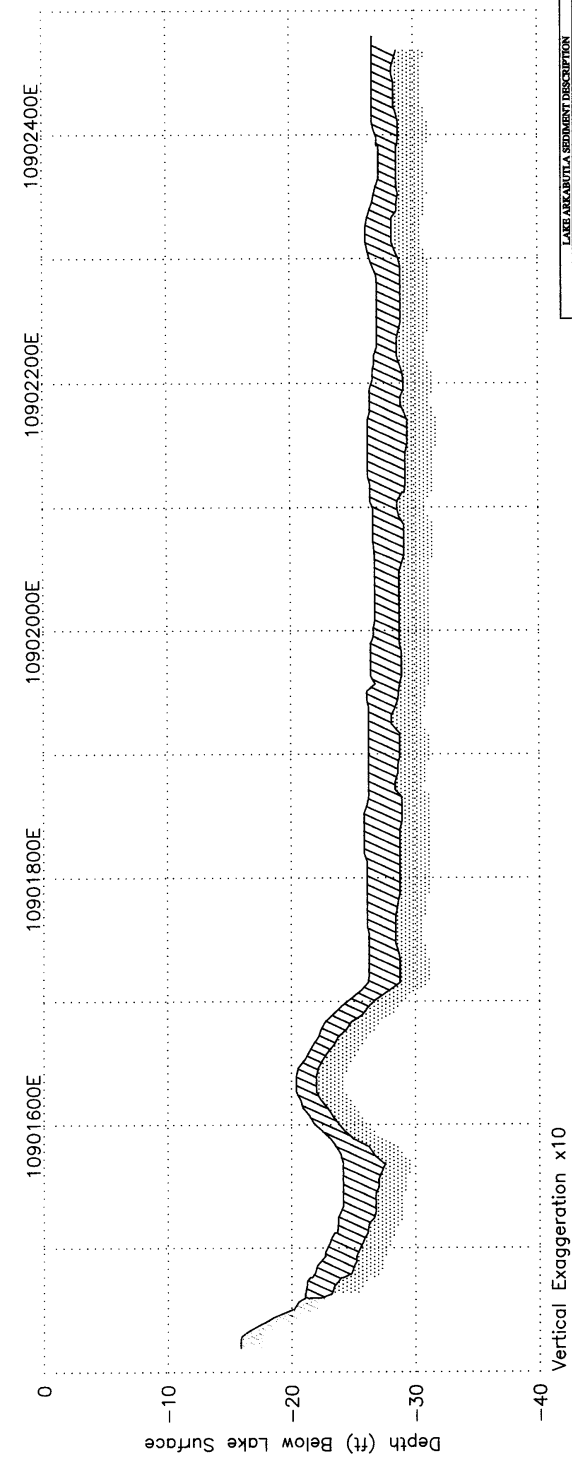
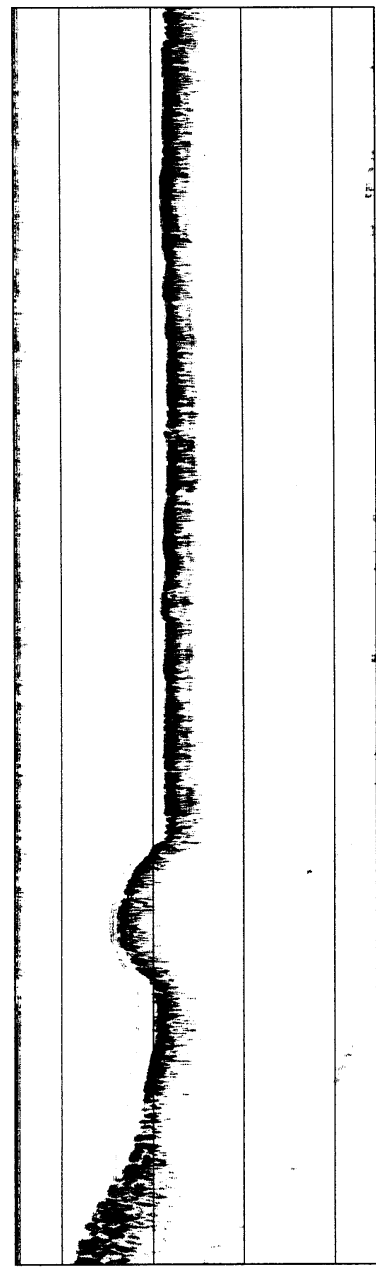
Figure 25. Sediment profile, Line 21.



**EVANS-HAMILTON, INC.**  
APPLIED SEISMICITY AND SURVEILLANCE  
4000 Union Bay Place N.E.  
Seattle, WA 98105-4025  
Ph: (206) 726-5022

**Navigation Software**  
Program: **SEISVIEW**  
Version: **1.0**  
UTM  
Zone: **18N**  
Datum: **WGS84**  
Spheroid: **WGS84**  
Units: **U.S. Survey Feet**  
Survey: **March, 1999**  
Scale: **1" = 100'**  
Surveyed by: **Richard McCoy**  
Checked by: **Richard McCoy**  
Date: **June, 1998**  
Job No.: **4700.39**  
Sheet No.: **1**  
Scale No.: **1**

**Reservoir Seismic Mapping**  
**Arkabutla Lake,**  
**DeSoto County, MS**  
**3.5 kHz Profiles**  
**Line 32**



LAYER ARKABUTLA SEDIMENT DESCRIPTION	
Hatch Pattern	Density g/cm <sup>3</sup>
	< 1.2
	1.2 - 1.4
	1.4 - 1.7
	1.7 - 2.0
	2.0 - 2.2
	N/A

Figure 26. Sediment profile, Line 32.

# **Appendix A**

## **1-kHz Subbottom Profile Data**

---

F:\AR010000.DAT Ping=3150

F:\AR010000.DAT Ping=2939

F:\AR010000.DAT Ping=2728

F:\AR010000.DAT Ping=2517

F:\AR010000.DAT Ping=2307

F:\AR010000.DAT Ping=2096

F:\AR010000.DAT Ping=1885

F:\AR010000.DAT Ping=1674

F:\AR010000.DAT Ping=1464

F:\AR010000.DAT Ping=1253

F:\AR010000.DAT Ping=1042

F:\AR010000.DAT Ping=831

F:\AR010000.DAT Ping=621

F:\AR010000.DAT Ping=410

F:\AR010000.DAT Ping=200

F:\AR010000.DAT Ping=3361

F:\AR010000.DAT Ping=3571

F:\AR010000.DAT Ping=3782

F:\AR010000.DAT Ping=3993

F:\AR010000.DAT Ping=4204

F:\AR010000.DAT Ping=4415

F:\AR010000.DAT Ping=4625

F:\AR010000.DAT Ping=4836

F:\AR010000.DAT Ping=5047

F:\AR010000.DAT Ping=5258

F:\AR010000.DAT Ping=5469

F:\AR010000.DAT Ping=5680

F:\AR010000.DAT Ping=5891

F:\AR010000.DAT Ping=6102

F:\ARR010010.DAT	Ping=2959	
F:\ARR010010.DAT	Ping=2710	
F:\ARR010010.DAT	Ping=2459	
F:\ARR010010.DAT	Ping=2209	
F:\ARR010010.DAT	Ping=1960	
F:\ARR010010.DAT	Ping=1710	
F:\ARR010010.DAT	Ping=1459	
F:\ARR010010.DAT	Ping=1209	
F:\ARR010010.DAT	Ping=960	
F:\ARR010010.DAT	Ping=710	
F:\ARR010010.DAT	Ping=460	
F:\ARR010010.DAT	Ping=210	

F:\AR010011.DAT Ping=8

A5

F:\AR010010.DAT Ping=5957

F:\AR010010.DAT Ping=5708

F:\AR010010.DAT Ping=5458

F:\AR010010.DAT Ping=5208

F:\AR010010.DAT Ping=4958

F:\AR010010.DAT Ping=4708

F:\AR010010.DAT Ping=4458

F:\AR010010.DAT Ping=4209

F:\AR010010.DAT Ping=3958

F:\AR010010.DAT Ping=3709

F:\AR010010.DAT Ping=3459

F:\AR010011.DAT Ping=256

F:\AR010011.DAT Ping=499

F:\AR010011.DAT Ping=742

F:\AR010011.DAT Ping=982

F:\AR010011.DAT Ping=1224



# **Appendix B**

## **4-kHz Subbottom Profile**

### **Records**

---

F:\AR040000.DAT Ping=217

F:\AR040000.DAT Ping=696

F:\AR040000.DAT Ping=1178

F:\AR040000.DAT Ping=1657

F:\AR040000.DAT Ping=2137

F:\AR040000.DAT Ping=2616

F:\AR040000.DAT Ping=3096

F:\AR040000.DAT Ping=3578

F:\AR040000.DAT Ping=4057

F:\AR040000.DAT Ping=4536

F:\AR040000.DAT Ping=5016

F:\AR040000.DAT Ping=5496

F:\AR040000.DAT Ping=5976

F:\AR040001.DAT Ping=249

F:\AR040001.DAT Ping=730

F:\AR040001.DAT Ping=1210

F:\AR040001.DAT Ping=1690

F:\AR040001.DAT Ping=2170

F:\AR040001.DAT Ping=2649

F:\AR040001.DAT Ping=3129

F:\AR040001.DAT Ping=3609

F:\AR040001.DAT Ping=4089

F:\AR040001.DAT Ping=4569

F:\AR040001.DAT Ping=5051

F:\AR040001.DAT Ping=5529

F:\AR040001.DAT Ping=6009

F:\AR040002.DAT Ping=282

B5

F:\AR040003.DAT P1ng=85

F:\AR040003.DAT P1ng=564

F:\AR040003.DAT P1ng=1044

F:\AR040003.DAT P1ng=1527

F:\AR040003.DAT P1ng=2005

F:\AR040003.DAT P1ng=2484

F:\AR040003.DAT P1ng=2964

F:\AR040003.DAT Ping=3444

F:\AR040003.DAT Ping=3924

F:\AR040003.DAT Ping=4404

F:\AR040003.DAT Ping=4884

F:\AR040003.DAT Ping=5363

F:\AR040003.DAT Ping=5844

F:\AR040004.DAT Ping=119

B7

F:\AR040004.DAT PInG=3477

F:\AR040004.DAT PInG=3957

F:\AR040004.DAT PInG=4437

F:\AR040004.DAT PInG=4919

F:\AR040004.DAT PInG=5396

F:\AR040004.DAT PInG=5876



F:\AR040005.DAT Plng=3153

B9

F:\AR040005.DAT Plng=2673

F:\AR040005.DAT Plng=2193

F:\AR040005.DAT Plng=1712

F:\AR040005.DAT Plng=1233

F:\AR040005.DAT Plng=753

F:\AR040005.DAT P1ng=3632

F:\AR040005.DAT P1ng=4114

F:\AR040005.DAT P1ng=4593

F:\AR040005.DAT P1ng=5072

F:\AR040005.DAT P1ng=5552

F:\AR040005.DAT P1ng=6032

F:\AR040006.DAT Ping=306

F:\AR040006.DAT Ping=786

F:\AR040006.DAT Ping=1266

F:\AR040006.DAT Ping=1746

F:\AR040006.DAT Ping=2226

F:\AR040006.DAT Ping=2705

B11

F:\AR040006.DAT Ping=3186

F:\AR040006.DAT Ping=3666

F:\AR040006.DAT Ping=4145

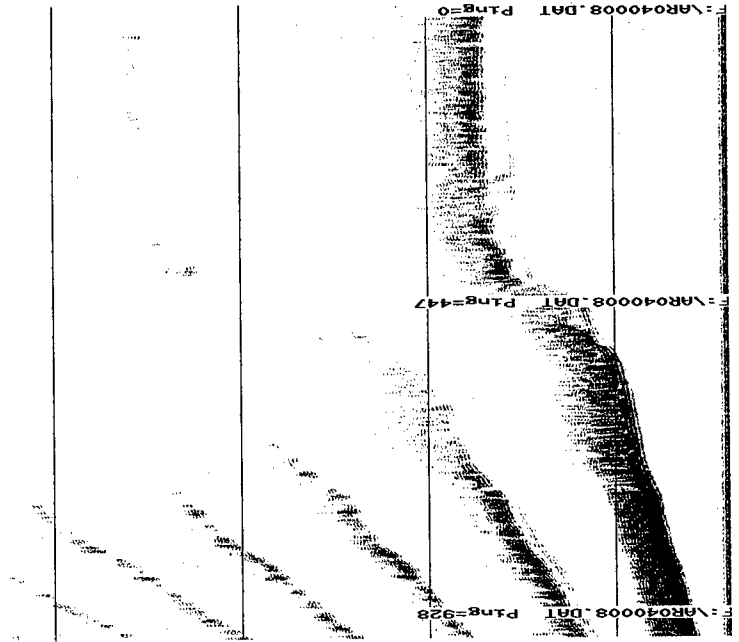
F:\AR040006.DAT Ping=4625

F:\AR040006.DAT Ping=5106

F:\AR040007.DAT Ping=178

F:\AR040007.DAT Ping=658

F:\AR040007.DAT Ping=1137



\\AR040009.DAT Ping=0  
\\AR040009.DAT Ping=230  
\\AR040009.DAT Ping=710

:\AR040010.DAT P1nr=0  
:\AR040010.DAT P1nr=323  
:\AR040010.DAT P1nr=803



\\AR040011.DAT Ping=0  
\\AR040011.DAT Ping=274  
\\AR040011.DAT Ping=754

:\AR040012.DAT Ping=0  
:\AR040012.DAT Ping=123  
:\AR040012.DAT Ping=602  
:\AR040012.DAT Ping=1083

\\ARO40013.DAT Plng=0  
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\\ARO40013.DAT Plng=897

F:\AR040014.DAT Ping=0  
F:\AR040014.DAT Ping=117  
F:\AR040014.DAT Ping=597  
F:\AR040014.DAT Ping=1078

F:\AR040015.DAT Plug=0  
F:\AR040015.DAT Plug=92  
F:\AR040015.DAT Plug=571

F:\AR040016.DAT Ping=0

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F:\AR040016.DAT Ping=922

F:\AR040017.DAT Ping=0

F:\AR040017.DAT Ping=259

F:\AR040018.DAT Plng=0

F:\AR040018.DAT Plng=449

F:\AR040018.DAT Plng=929



F:\AR040019.DAT Ping=0

F:\AR040019.DAT Ping=263

F:\AR040019.DAT Ping=742

F:\AR040019.DAT Ping=1222

F:\AR040020.DAT P1ng=0  
F:\AR040020.DAT P1ng=200  
F:\AR040020.DAT P1ng=680  
F:\AR040020.DAT P1ng=1159

F:\AR040021.DAT Ping=0  
F:\AR040021.DAT Ping=36  
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F:\AR040021.DAT Ping=996

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F:\AR040021.DAT Ping=516  
F:\AR040021.DAT Ping=996

F:\AR040021.DAT P1ng=1475  
F:\AR040022.DAT P1ng=37  
F:\AR040022.DAT P1ng=517  
F:\AR040022.DAT P1ng=996

F:\AR040023.DAT Plng=0

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F:\AR040023.DAT Plng=359

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F:\AR040024.DAT Ping=0  
F:\AR040024.DAT Ping=238  
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F:\AR040024.DAT Ping=1198

F:\AR040025.DAT P118=0  
F:\AR040025.DAT P118=106  
F:\AR040025.DAT P118=587  
F:\AR040025.DAT P118=1066  
F:\AR040025.DAT P118=1546

F:\AR040026.DAT P1ng=0

F:\AR040026.DAT P1ng=195

F:\AR040026.DAT P1ng=672

F:\AR040026.DAT P1ng=1152



F:\AR040027.DAT Ping=0  
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F:\AR040027.DAT Ping=1049  
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F:\AR040030.DAT P1ng=1285

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F:\AR040031.DAT Ping=1817

F:\AR040032.DAT Ping=424

F:\AR040032.DAT Ping=904

F:\AR040032.DAT Ping=1383

F:\AR040033.DAT Ping=57

F:\AR040033.DAT Ping=535

F:\AR040033.DAT Ping=1015

F:\AR040034.DAT Ping=0

F:\AR040034.DAT Ping=141

F:\AR040034.DAT Ping=620

F:\AR040034.DAT Ping=1100



F:\AR040035.DAT Ping=148

F:\AR040035.DAT Ping=628

F:\AR040035.DAT Ping=1107

F:\AR040036.DAT Plng=340

F:\AR040036.DAT Plng=819

F:\AR040037.DAT Ping=454

F:\AR040037.DAT Ping=934

F:\AR040038.DAT Plng=221

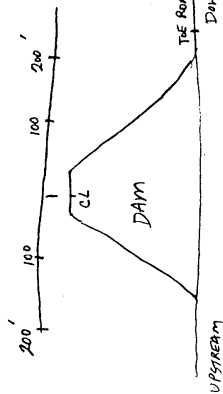
F:\AR040038.DAT Plng=700

# **Appendix C**

## **Available Core Information**

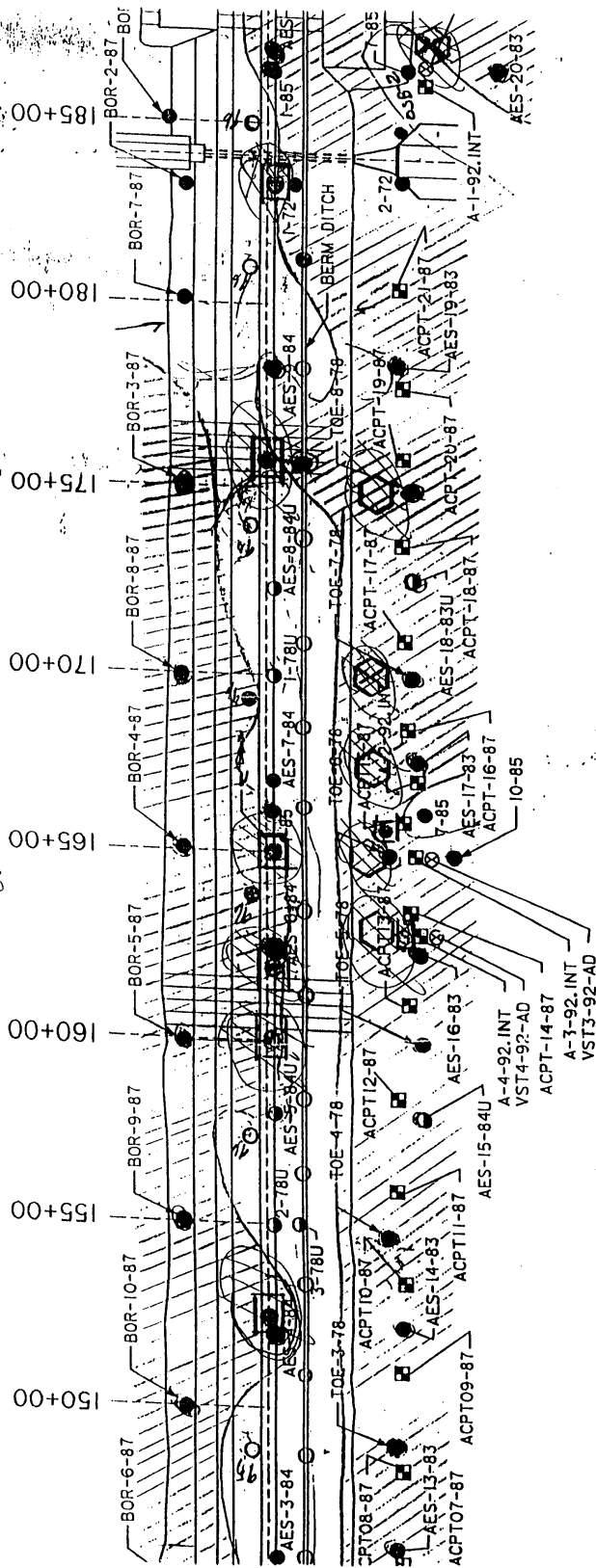
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# ARKABUTLA DAM

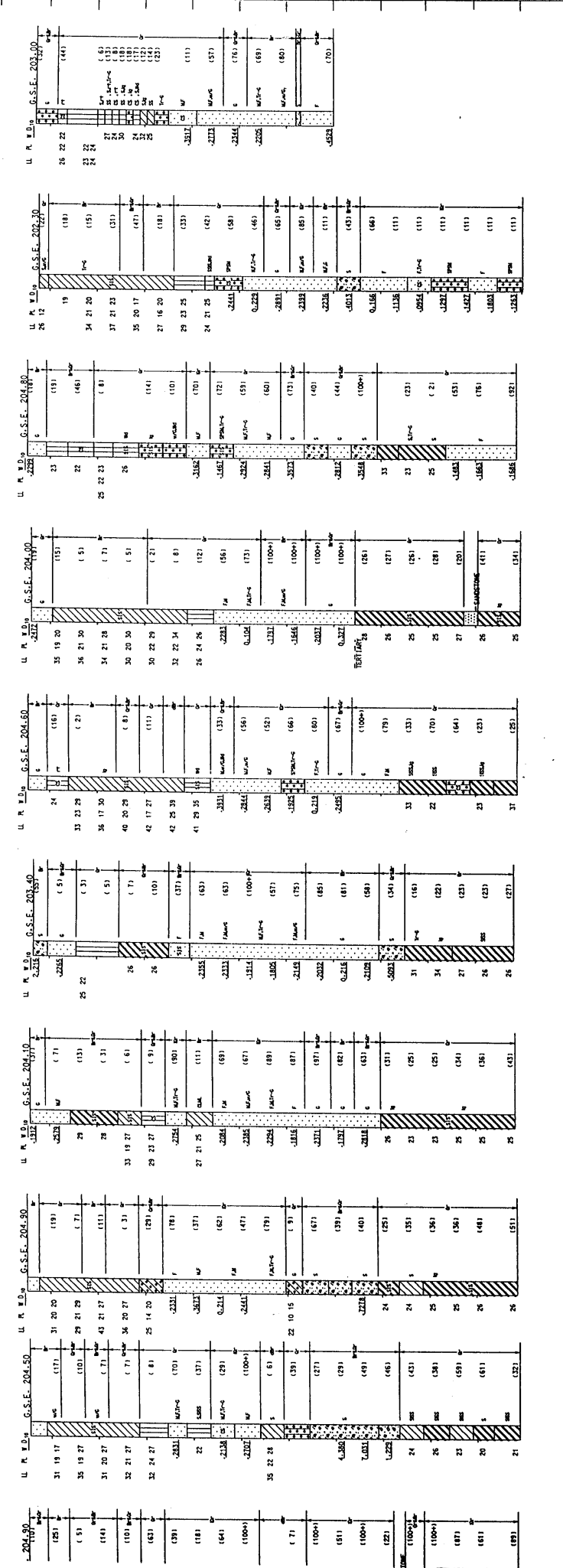


## UPSTREAM

ALL BORINGS NAMED BOR-X-87 ARE LOCATED IN THE WATER NEAR THE TOE - APPROXIMATELY 200' OFF CENTER LINE OF DAM. AND NEAR OF CONTROL STRUCTURE.



6-87 BOR-1-87 BOR-2-87 BOR-3-87 BOR-4-87 BOR-5-87 BOR-9-87 BOR-10-87  
 185+10 183+03 180+00 175+00 170+00 165+00 160+00  
 262' US CL OF DAM 217' US CL DAM 215' US FROM CL DAM 221' US CL OF DAM 225' US FROM CL DAM 215' US FROM CL DAM 215' US FROM CL DAM  
 19 AUG 87 10 SEP 87 25 AUG 87 14 SEP 87 31 AUG 87 3 SEP 87 15 SEP 87 16 SEP 87



[illegible]



	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB	AC	AD	AE	AF	AG
75	04-31-87	BOR-04-15	20	215	182.4	181.9													10														
76	04-31-87	BOR-04-16	25	26.5	178.4	176.9	28.5												37														
77	04-31-87	BOR-04-17	30	11.5	174.4	171.9	33.0												63														
78	04-31-87	BOR-04-18	35	34	168.4	166.9													89														
79	04-31-87	BOR-04-19	40	41.5	163.4	161.9													100														
80	04-31-87	BOR-04-20	45	46.5	158.4	156.9													127														
81	04-31-87	BOR-04-21	50	51.5	153.4	151.9													154														
82	04-31-87	BOR-04-22	55	56	148.4	146.9													181														
83	04-31-87	BOR-04-23	60	60.9	143.4	141.9													208														
84	04-31-87	BOR-04-24	65	65.9	138.4	136.9	73.0												235														
85	04-31-87	BOR-04-25	70	70.9	133.4	131.9													262														
86	04-31-87	BOR-04-26	75	75.9	128.4	126.9	78.5												289														
87	04-31-87	BOR-04-27	80	81.5	123.4	121.9	81.0												316														
88	04-31-87	BOR-04-28	85	86.5	118.4	116.9	83.5												343														
89	04-31-87	BOR-04-29	90	91.5	113.4	111.9	86.0												370														
90	04-31-87	BOR-04-30	95	96.5	108.4	106.9													397														
91	04-31-87	BOR-04-31	100	101.5	103.4	101.9	101.5												424														
92	04-31-87	BOR-04-32	105	106.5	98.4	96.9													451														
93	04-31-87	BOR-04-33	110	111.5	93.4	91.9	8.5												478														
94	04-31-87	BOR-04-34	115	116.5	88.4	86.9													505														
95	04-31-87	BOR-04-35	120	121.5	83.4	81.9	15.5												532														
96	04-31-87	BOR-04-36	125	126.5	78.4	76.9													559														
97	04-31-87	BOR-04-37	130	131.5	73.4	71.9													586														
98	04-31-87	BOR-04-38	135	136.5	68.4	66.9													613														
99	04-31-87	BOR-04-39	140	141.5	63.4	61.9													640														
100	04-31-87	BOR-04-40	145	146.5	58.4	56.9													667														
101	04-31-87	BOR-04-41	150	151.5	53.4	51.9													694														
102	04-31-87	BOR-04-42	155	156.5	48.4	46.9													721														
103	04-31-87	BOR-04-43	160	161.5	43.4	41.9													748														
104	04-31-87	BOR-04-44	165	166.5	38.4	36.9													775														
105	04-31-87	BOR-04-45	170	171.5	33.4	31.9													802														
106	04-31-87	BOR-04-46	175	176.5	28.4	26.9													829														
107	04-31-87	BOR-04-47	180	181.5	23.4	21.9													856														
108	04-31-87	BOR-04-48	185	186.5	18.4	16.9													883														
109	04-31-87	BOR-04-49	190	191.5	13.4	11.9													910														
110	04-31-87	BOR-04-50	195	196.5	8.4	6.9													937														
111	04-31-87	BOR-04-51	200	201.5	3.4	1.9													964														
112	04-31-87	BOR-04-52	205	206.5	-2.4	-0.9													991														
113	04-31-87	BOR-04-53	210	211.5	-7.4	-5.9													1018														
114	04-31-87	BOR-04-54	215	216.5	-12.4	-10.9													1045														
115	04-31-87	BOR-04-55	220	221.5	-17.4	-15.9													1072														
116	04-31-87	BOR-04-56	225	226.5	-22.4	-20.9													1099														
117	04-31-87	BOR-04-57	230	231.5	-27.4	-25.9													1126														
118	04-31-87	BOR-04-58	235	236.5	-32.4	-30.9													1153														
119	04-31-87	BOR-04-59	240	241.5	-37.4	-35.9													1180														
120	04-31-87	BOR-04-60	245	246.5	-42.4	-40.9													1207														
121	04-31-87	BOR-04-61	250	251.5	-47.4	-45.9													1234														
122	04-31-87	BOR-04-62	255	256.5	-52.4	-50.9													1261														
123	04-31-87	BOR-04-63	260	261.5	-57.4	-55.9													1288														
124	04-31-87	BOR-04-64	265	266.5	-62.4	-60.9													1315														
125	04-31-87	BOR-04-65	270	271.5	-67.4	-65.9													1342														
126	04-31-87	BOR-04-66	275	276.5	-72.4	-70.9													1369														
127	04-31-87	BOR-04-67	280	281.5	-77.4	-75.9													1396														
128	04-31-87	BOR-04-68	285	286.5	-82.4	-80.9													1423														
129	04-31-87	BOR-04-69	290	291.5	-87.4	-85.9													1450														
130	04-31-87	BOR-04-70	295	296.5	-92.4	-90.9													1477														
131	04-31-87	BOR-04-71	300	301.5	-97.4	-95.9													1504														
132	04-31-87	BOR-04-72	305	306.5	-102.4	-100.9													1531														
133	04-31-87	BOR-04-73	310	311.5	-107.4	-105.9													1558														
134	04-31-87	BOR-04-74	315	316.5	-112.4	-110.9													1585														
135	04-31-87	BOR-04-75	320	321.5	-117.4	-115.9													1612														
136	04-31-87	BOR-04-76	325	326.5	-122.4	-120.9													1639														
137	04-31-87	BOR-04-77	330	331.5	-127.4	-125.9													1666														
138	04-31-87	BOR-04-78	335	336.5	-132.4	-130.9													1693														
139	04-31-87	BOR-04-79	340	341.5	-137.4	-135.9													1720														

[illegible]

A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AB	AC	AD	AE	AF	AG
205	00-15-87	BOR-10-4-15	70	71	124.5	133	79.5		GP								48			7.027	22.80	59.2	4.2	0.5								
206	00-15-87	BOR-10-4-15	75	79.5	125.5	127	79.0		GW								48			1.2289	8.17	74.1	24.8	1.1								
207	00-15-87	BOR-10-4-15	80	81.5	124.5	123	80.0		CL			24	40	14	26		43															
208	00-15-87	BOR-10-4-15	85	86.5	124.5	127	80.5		CL			25	40	14	26		43															
209	00-15-87	BOR-10-4-15	90	91.5	124.5	130	81.5		CL			23	44	14	30		58															
210	00-15-87	BOR-10-4-15	95	96.5	124.5	133	82.5		CL			20					61															
211	00-15-87	BOR-10-4-15	100	103.5	124.5	133	83.5		CH			21					52															

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<b>14. ABSTRACT</b> The need exists for development of in situ techniques for more accurately determining site conditions offshore of dams and levees in lakes and reservoirs within hazard areas. This report describes the use of a new data processing approach utilizing a Biot theory approach to assess acoustic sediment interactions in porous, saturated media. Ramifications of the Biot theory may aid engineering in accurately assessing liquefaction potential of Corps structures.							
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